

# Logarithmisch-Periodische Antennen

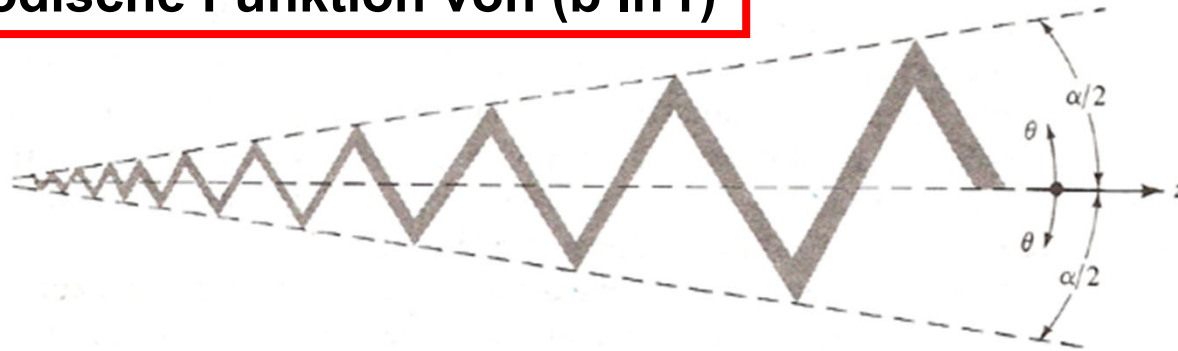
by Thomas Zwick

INSTITUT FÜR HOCHFREQUENZTECHNIK UND ELEKTRONIK

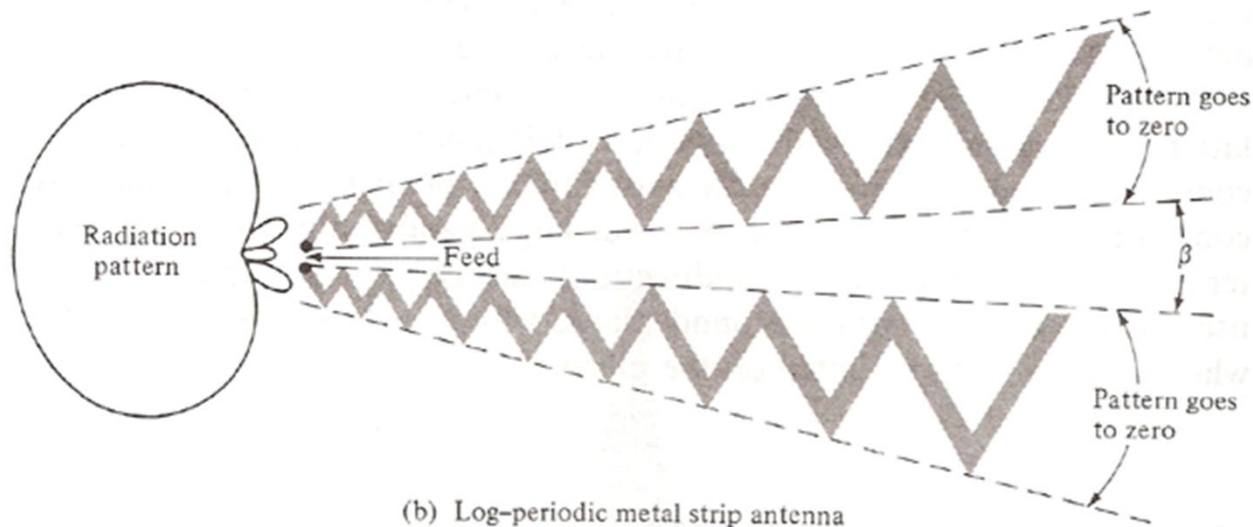


# Logarithmisch-Periodische Antenne (Log-Per-)

$\Theta$  = periodische Funktion von  $(b \ln r)$



(a) Metal strip log-periodic configuration

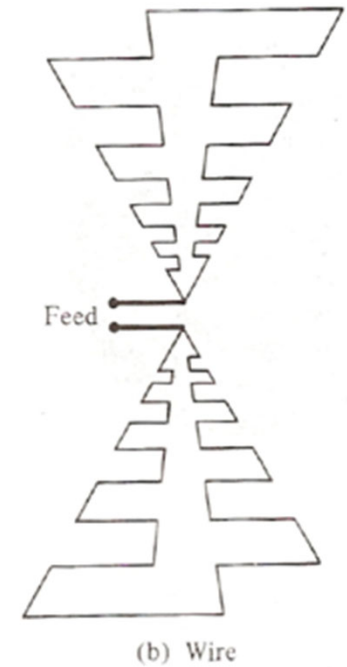
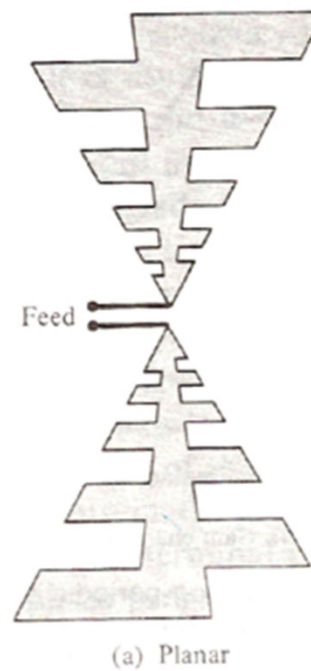
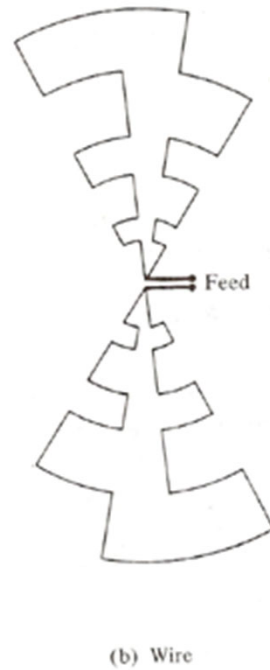
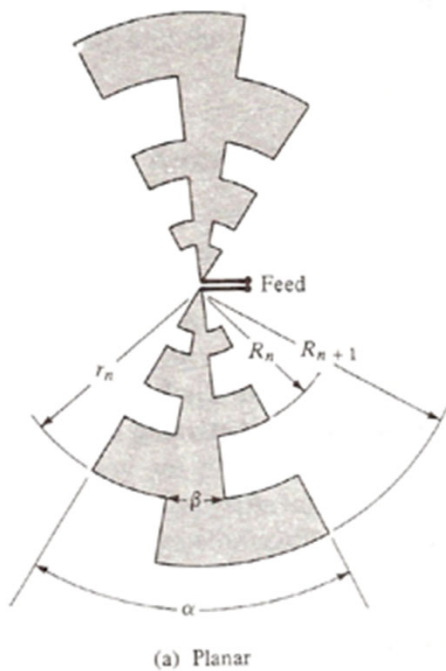


(b) Log-periodic metal strip antenna

Quelle: Antenna  
Theory (Balanis)

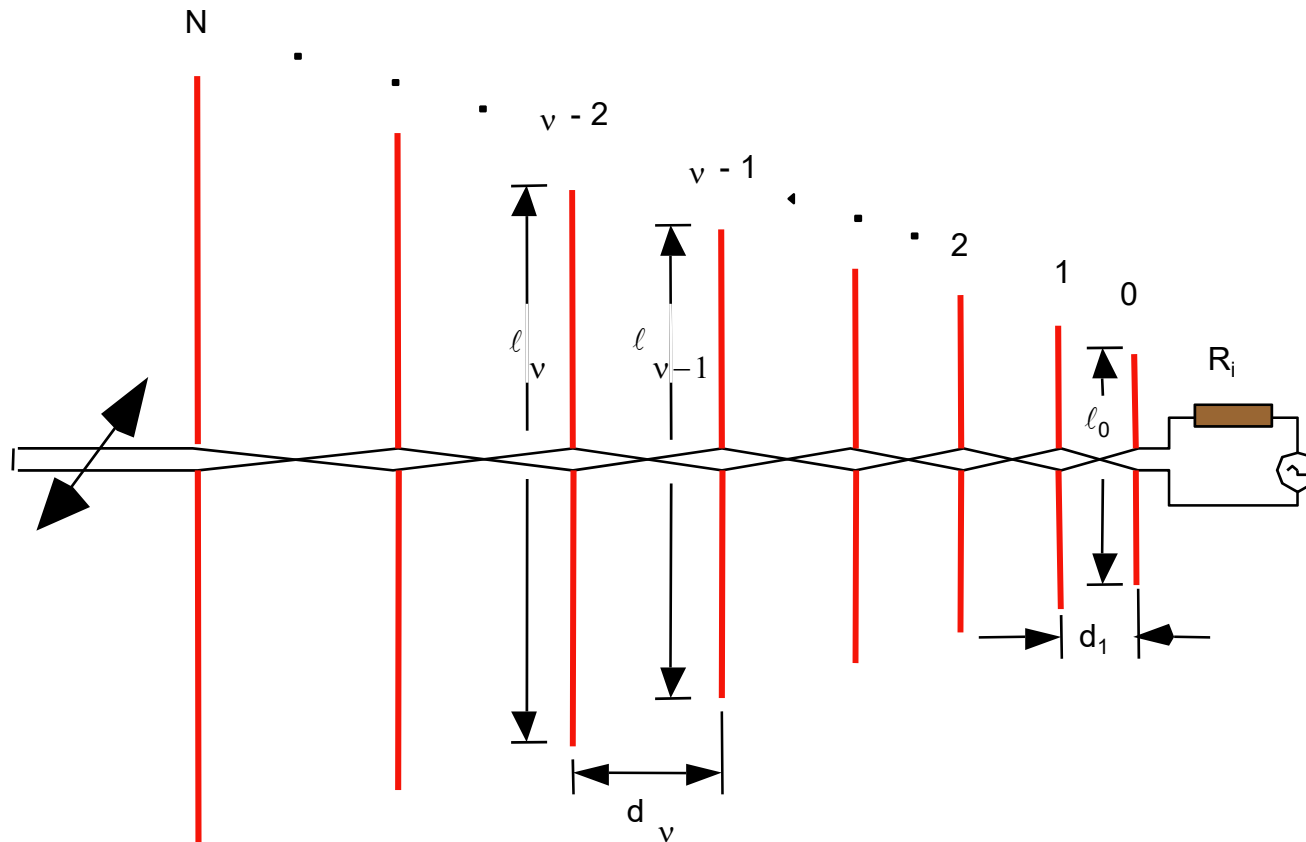
# Logarithmisch-Periodische Antenne (Log-Per)

$\Theta$  = periodische Funktion von  $(b \ln r)$



Quelle: Antenna Theory (Balanis)

# Logarithmisch-Periodisches Dipol-Array





# Log-Per-Dipolantenne

## 4 Designparameter:

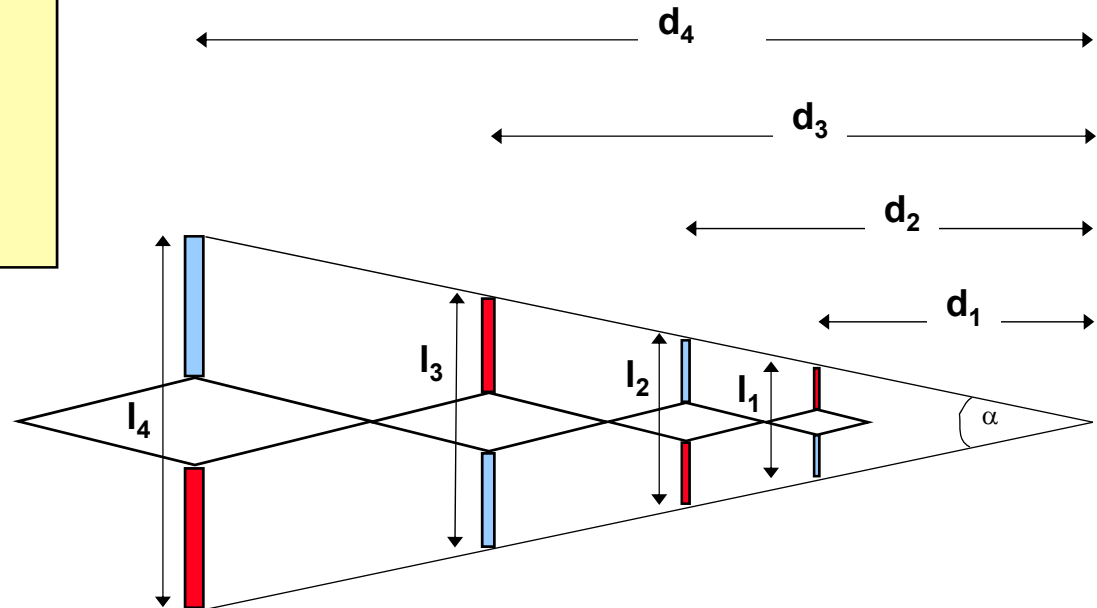
- $\hat{a}$  Dipolbreite  $w$
- $\hat{a}$  Dipollänge  $l$
- $\hat{a}$  Skalierungsfaktor  $\tau$
- $\hat{a}$  Abstand  $d$

$$\sigma = \frac{d_n}{2l_n}$$

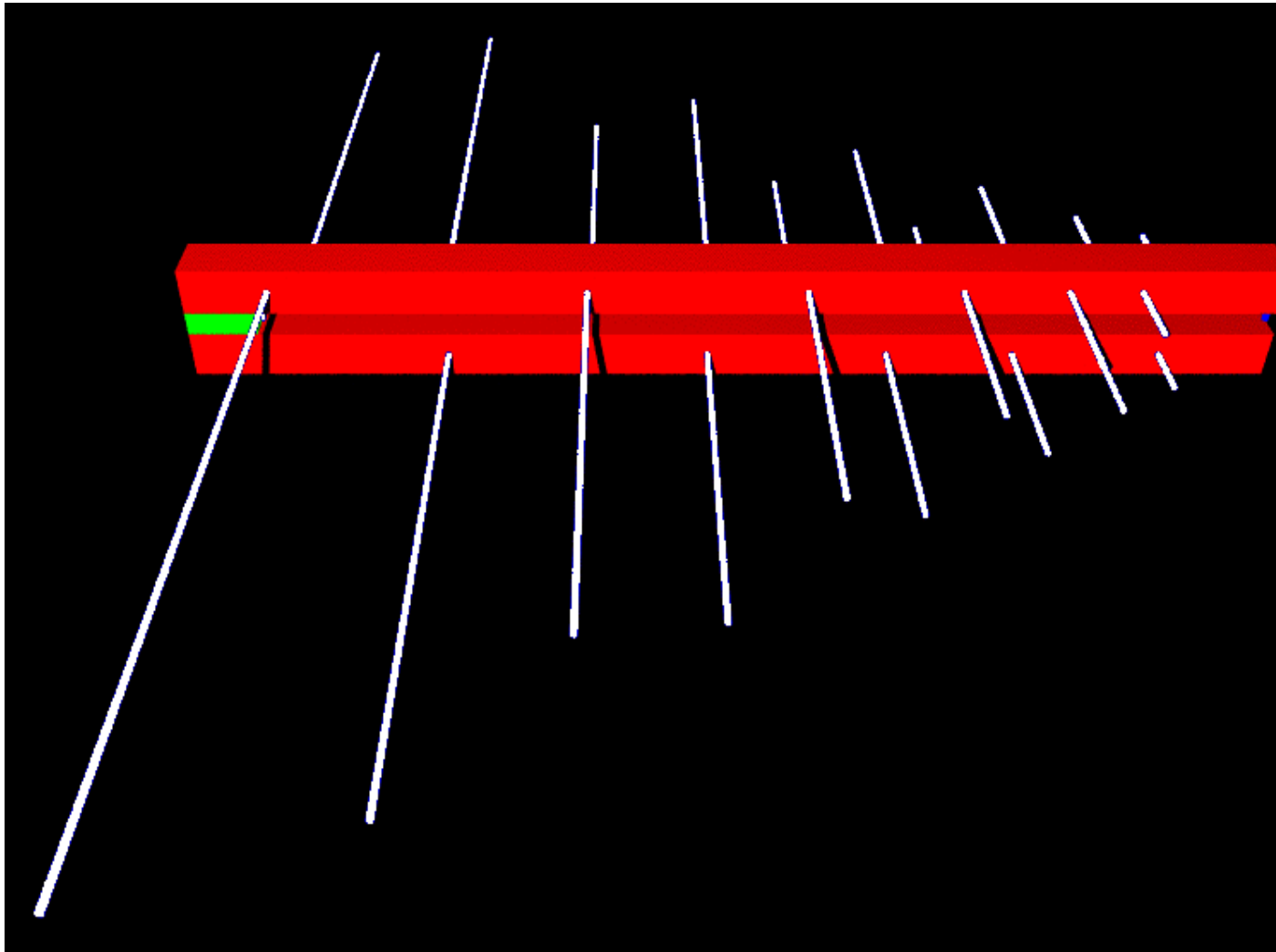
$$\alpha = 2 \arctan \left( \frac{1 - \tau}{4\sigma} \right)$$

$$\tau = \frac{l_1}{l_2} = \frac{l_n}{l_{n+1}} = \frac{d_1}{d_2} = \frac{d_n}{d_{n+1}} = \frac{w_1}{w_2} = \frac{w_n}{w_{n+1}}$$

$$\log \frac{l_v}{l_0} = v \cdot \log C$$



# Breitbandantennen (3)



# Realisierung für 3 - 10 GHz

## Vorgaben

Antenne für  
3 - 10 GHz

Bauweise:  
quadratisch  
kompakt

max. Gewinn

Anpassung,  
breitbandig

## Parameter

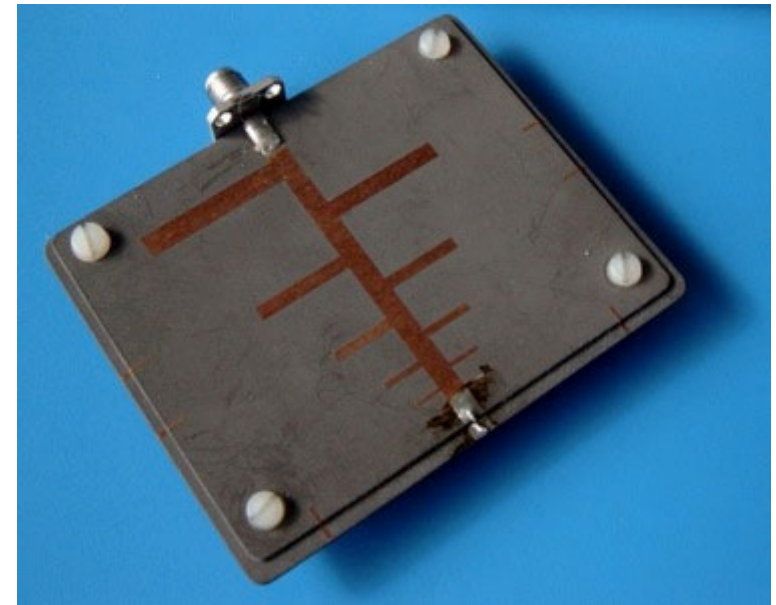
$L_N = 44.3 \text{ mm}$   
 $L_1 = 4.8 \text{ mm}$

$S = 44.3 \text{ mm}$

$\tau = 0,80$   
 $\sigma = 0,112$

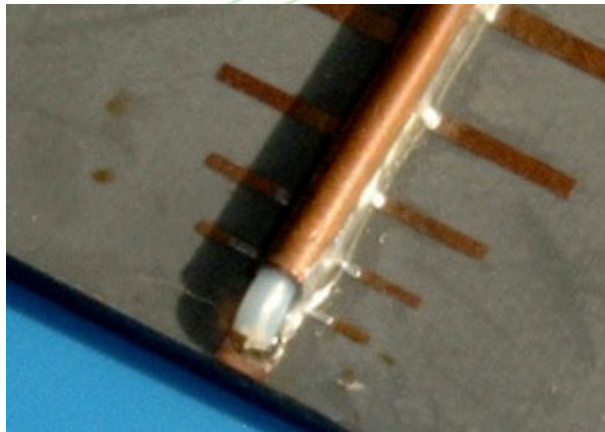
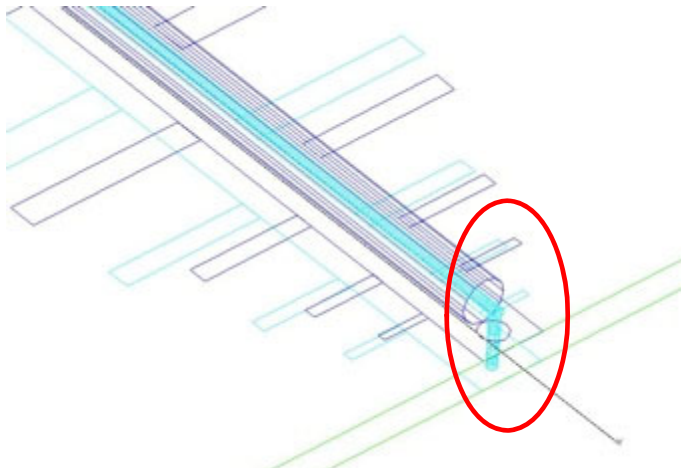
$N = 11$

$l/w = 12,5$

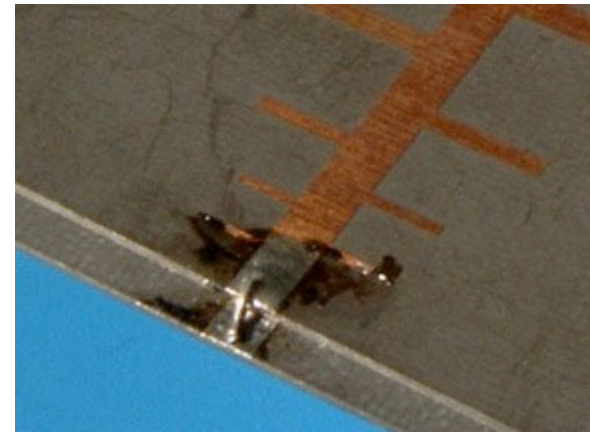
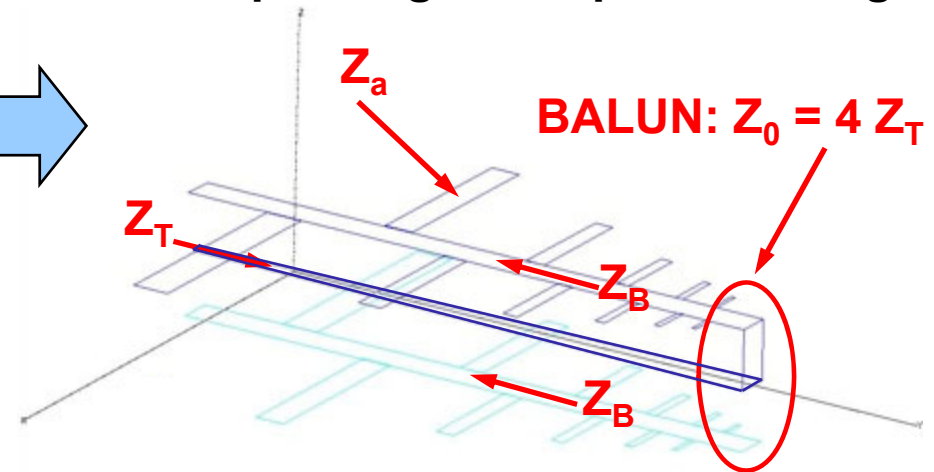
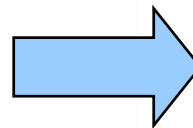


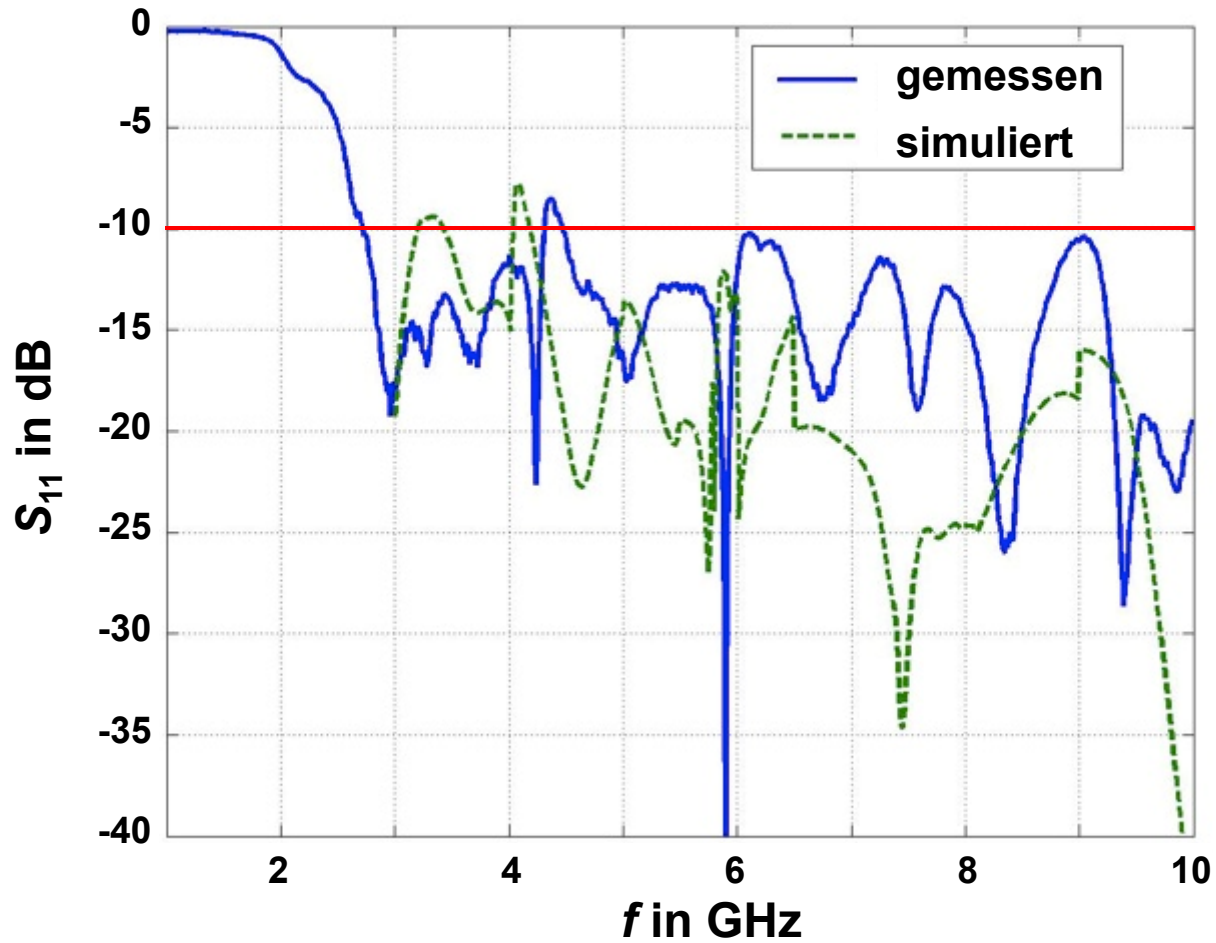
(Material: Duroid 5880,  $\epsilon_r = 2,2$ )

## übliche Speisemethode

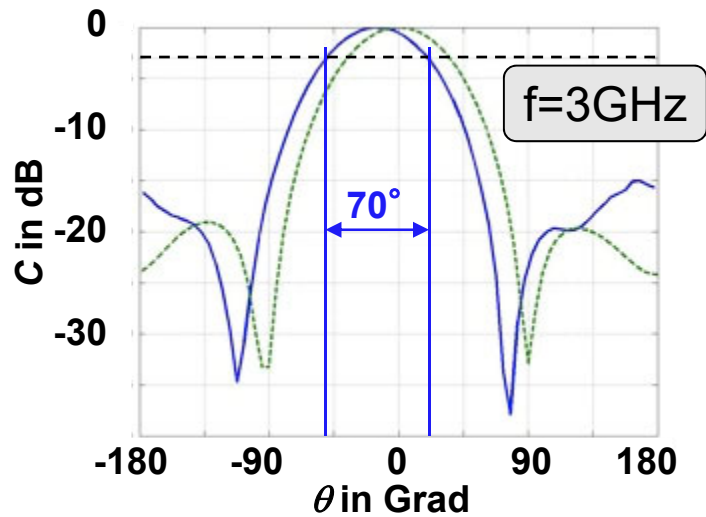


## Speisung mit Triplate-Leitung



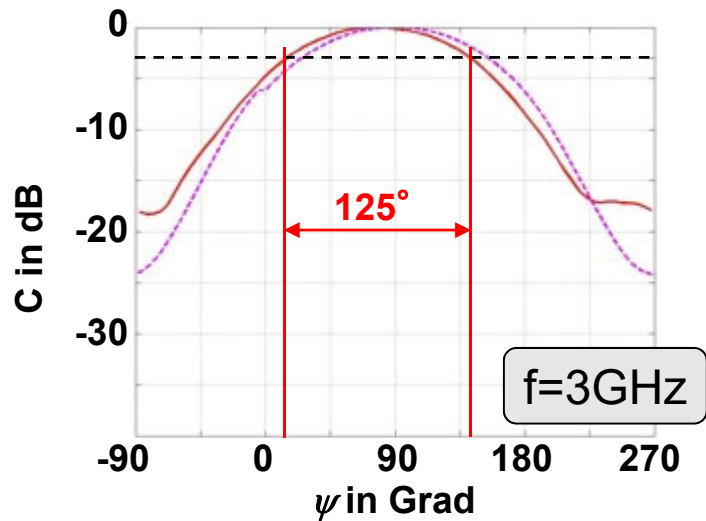


# Richtcharakteristiken $C(\theta, \psi)$



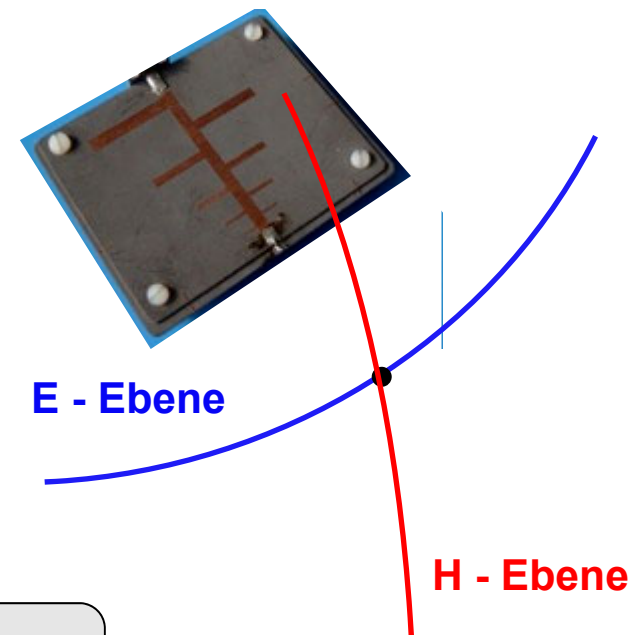
— gemessen  
- - - simuliert

**E - Ebene**



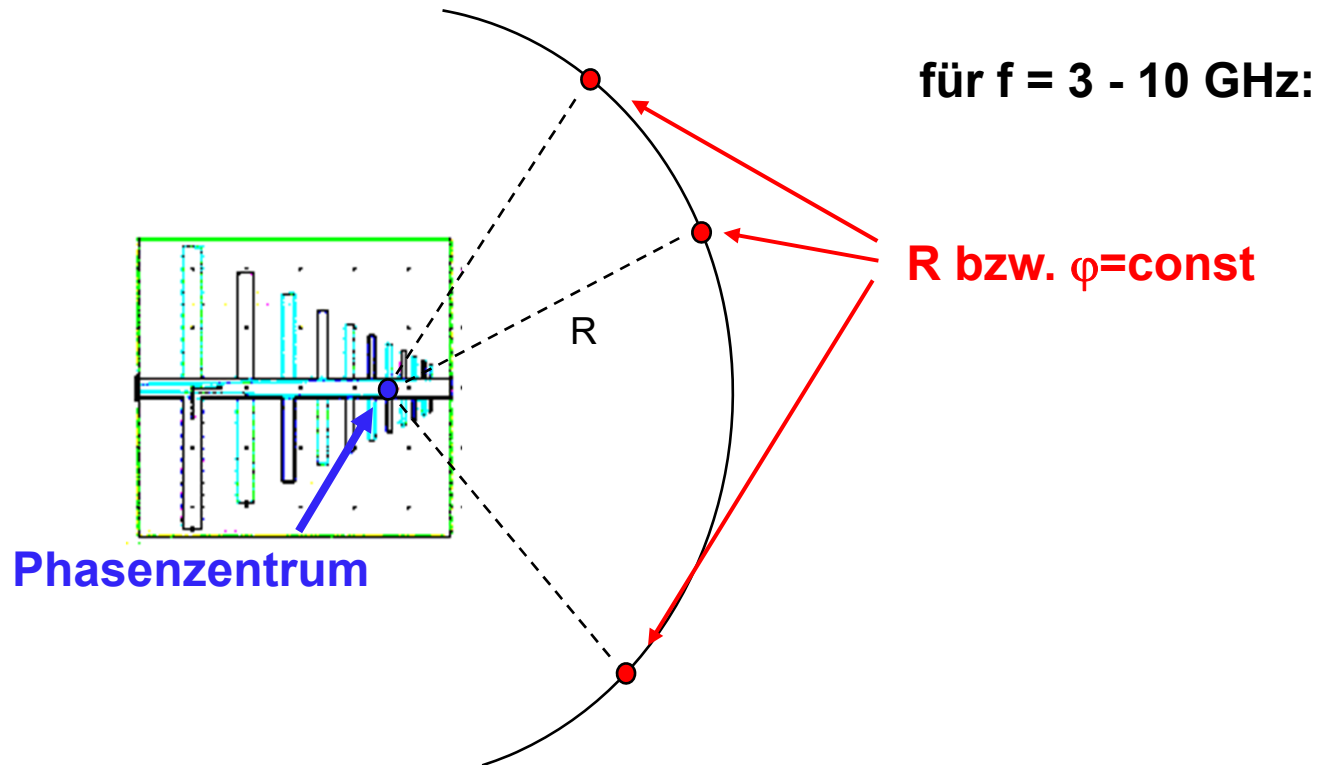
— gemessen  
- - - simuliert

**H - Ebene**

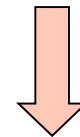




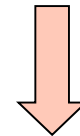
## Phasenzentrum: Ersatzkugelstrahler mit gegebener Richtcharakteristik



Phasenzentrum  
nicht konstant

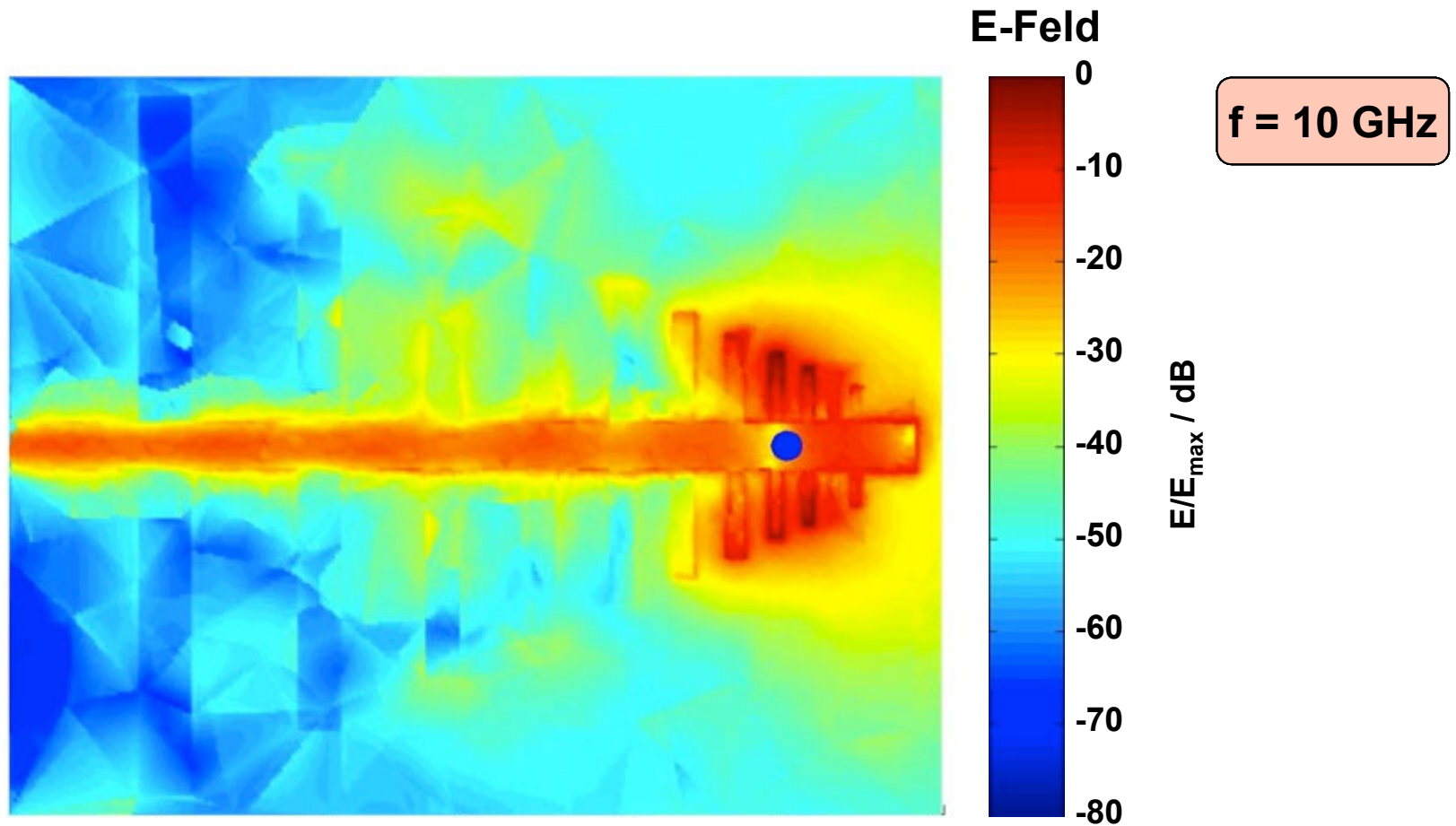


Zeitversatz

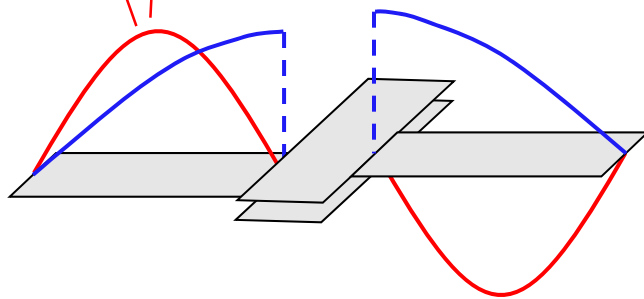
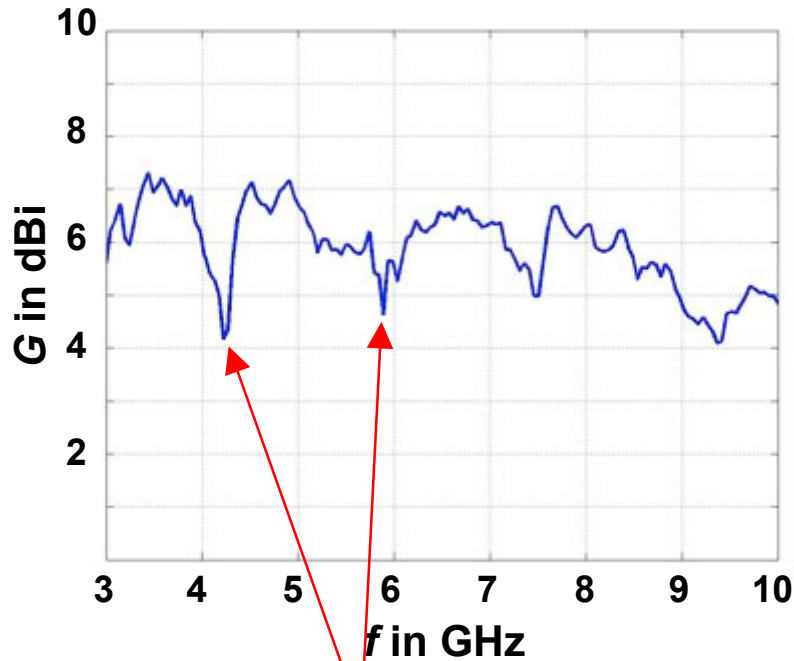


Dispersion

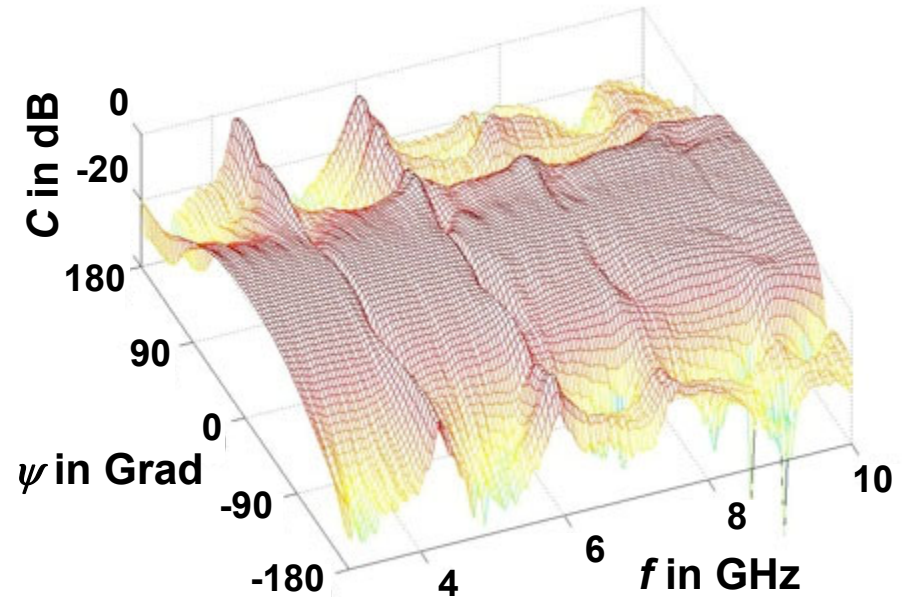
# Wanderndes Phasenzentrum



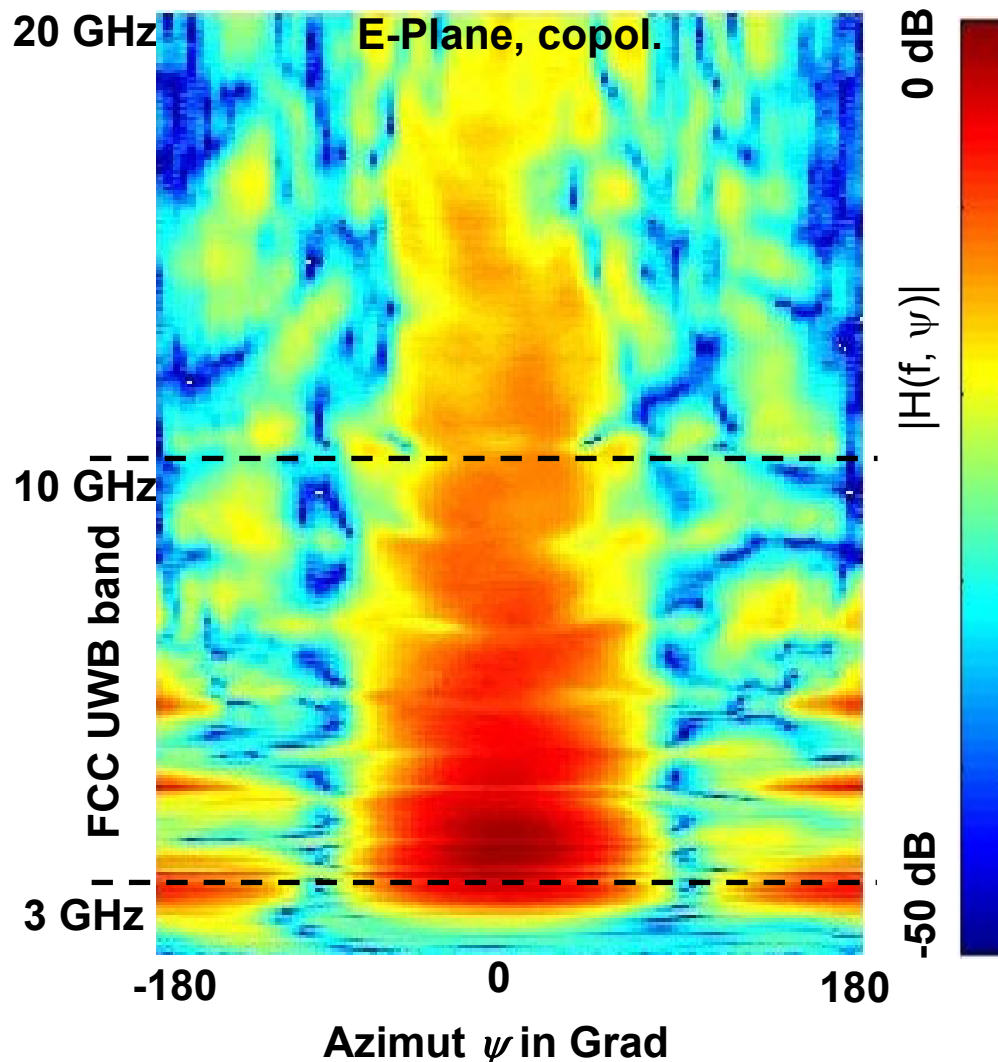
# Gewinn über dem Frequenzbereich



Richtcharakteristik  $f = 3 - 10$  GHz



# LogPer-Antennen Transfer Funktion $H_n$



Transfer function:

$$\vec{H}_n(f, \theta, \psi)$$

â linear model for radiated far field depends on:

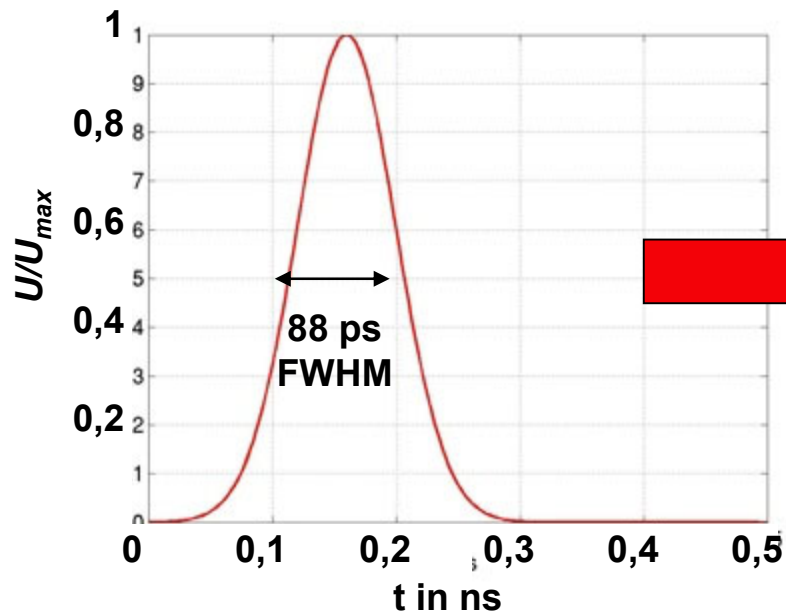
- direction
- polarization
- frequency

Antenna gain and transfer function:

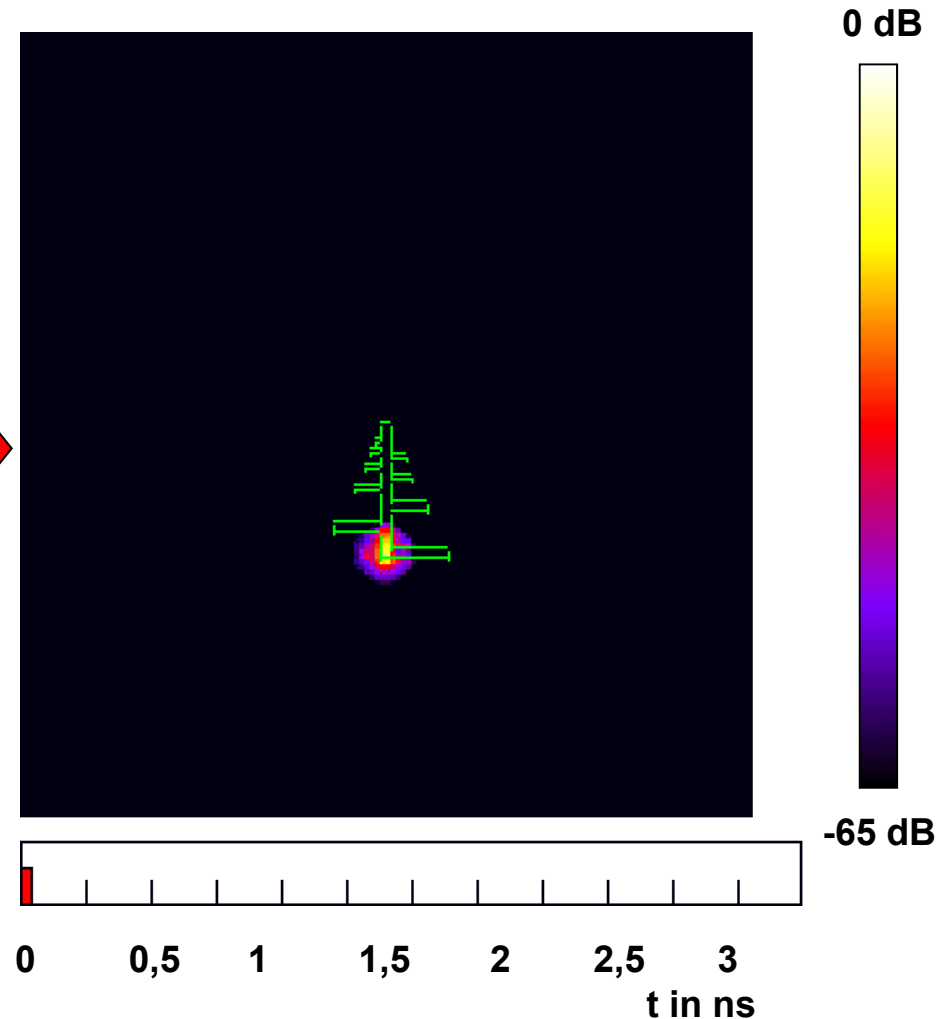
$$G(f, \theta, \psi) = \frac{4\pi f^2}{c^2} \left| \vec{H}_n(f, \theta, \psi) \right|^2$$

# Log-Per Antenna Simulation in Time Domain

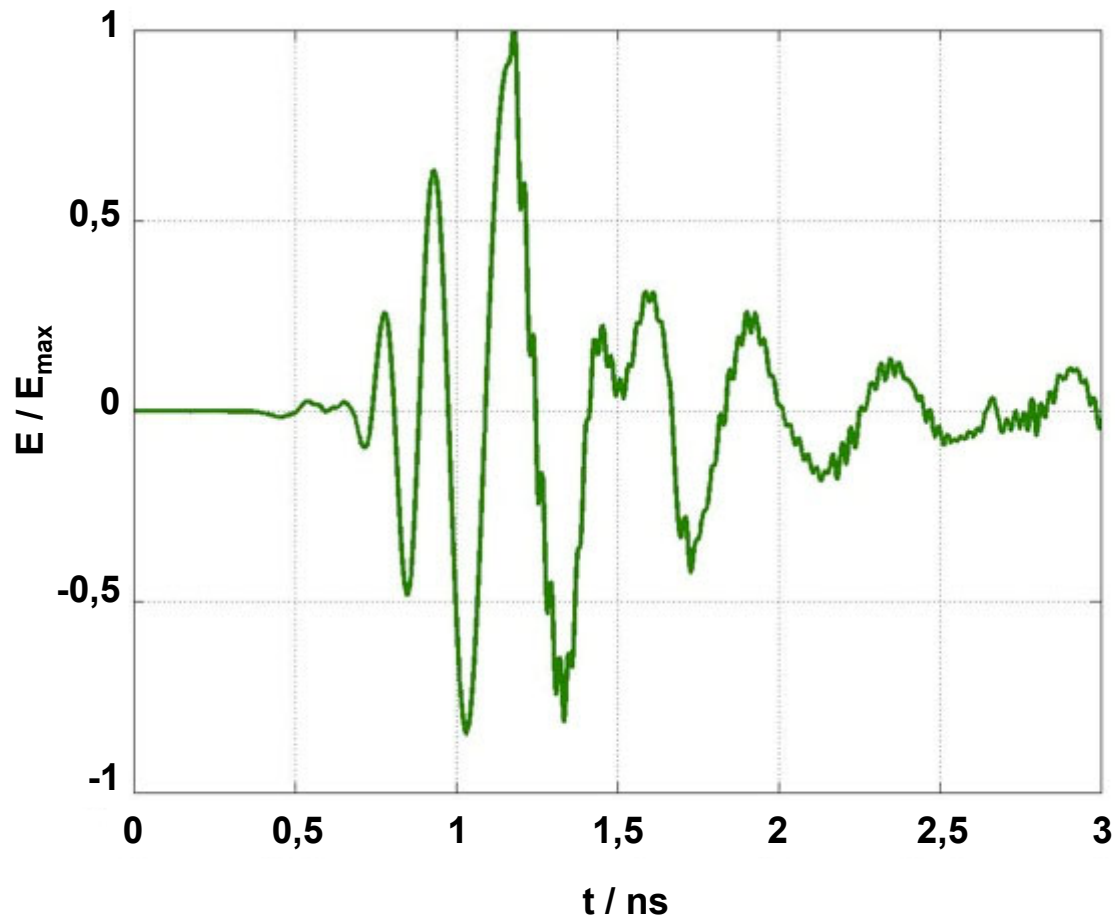
Normalized excitation voltage



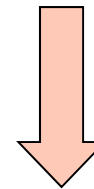
FWHM: Full Width at Half Maximum



# Zeitlicher Verlauf des E-Feldes

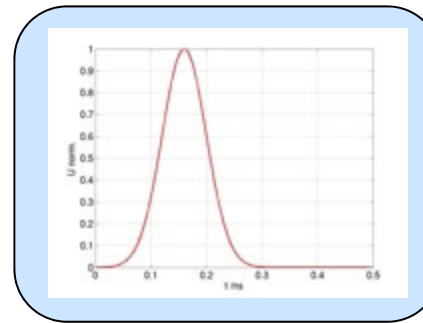


**Resonanzstruktur  
der Antenne**

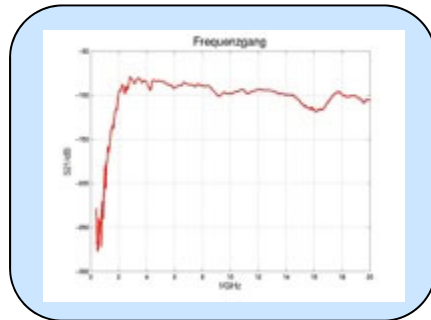


**Impulsfolge wird  
abgestrahlt**

# Transformation der Messdaten



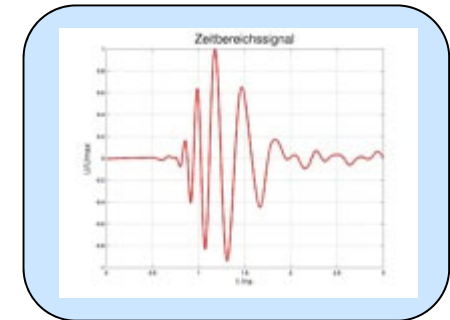
Anregungsfunktion  $U_0(t)$



Messung im Frequenzbereich  
(801 Frequenzpunkte)

FFT

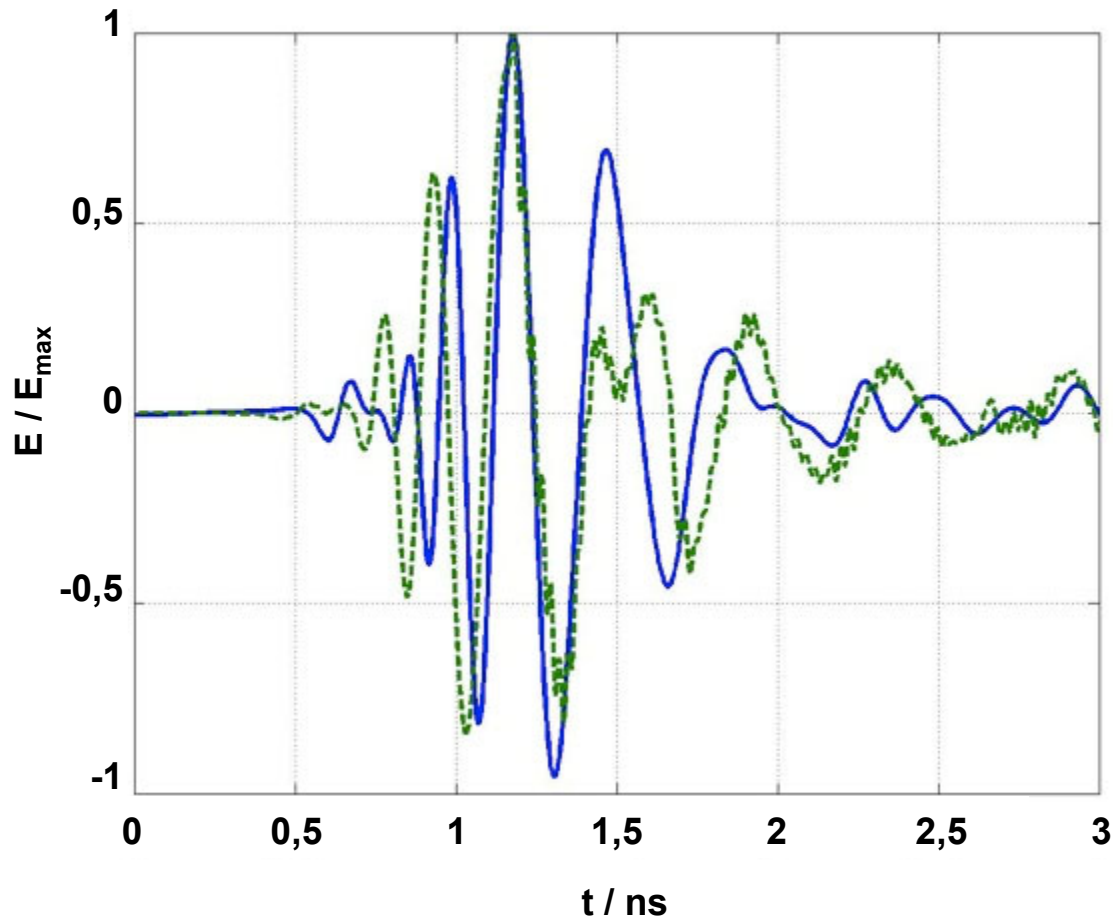
IFT



zeitlicher Verlauf  
der Feldstärke



# Vergleich Simulation $\Leftrightarrow$ Messung



— gemessener Feldverlauf  
- - - simulierter Feldverlauf

# Vivaldi Antennen

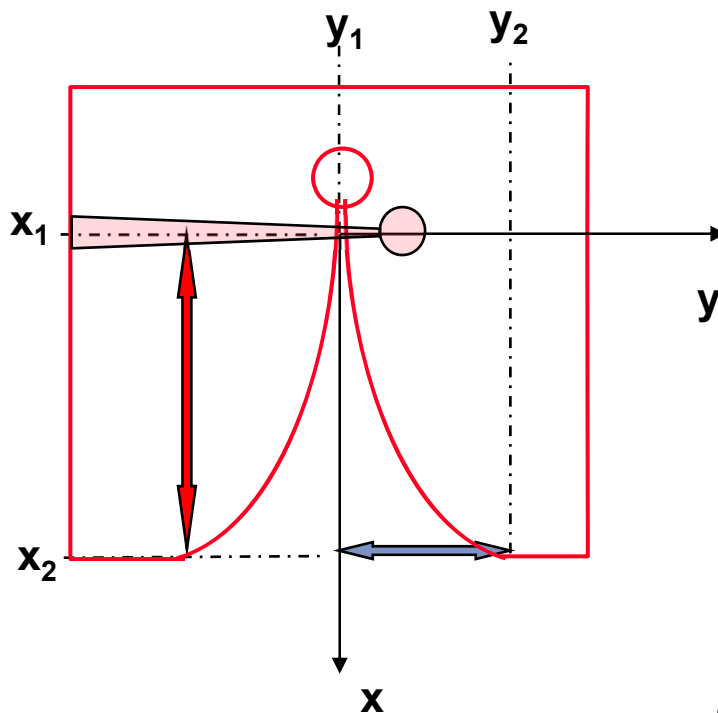
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# Vivaldi Antenna: Exponentially Tapered Slot Antenna

## Exponential taper design:



$$y(x) = A \cdot e^{Rx} + B \quad \text{with}$$

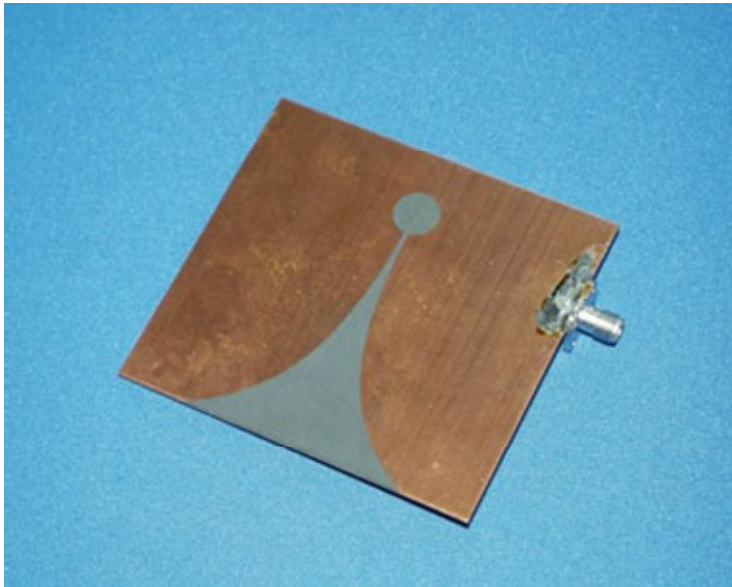
$$A = \frac{y_2 - y_1}{e^{Rx_2} - e^{Rx_1}}$$

$$B = \frac{y_1 \cdot e^{Rx_2} - y_2 \cdot e^{Rx_1}}{e^{Rx_2} - e^{Rx_1}}$$

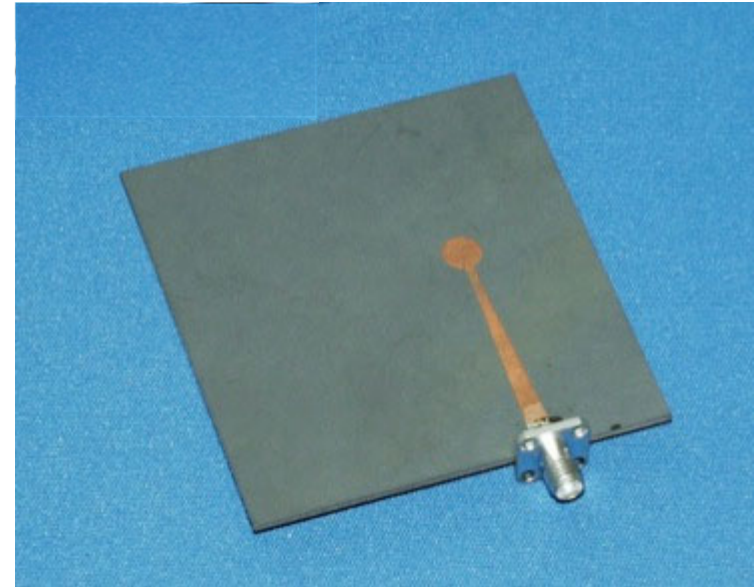
$$R = 0,8/\text{mm}$$

Opening Rate  $R$  determines curvature.

# Vivaldi-Antenna



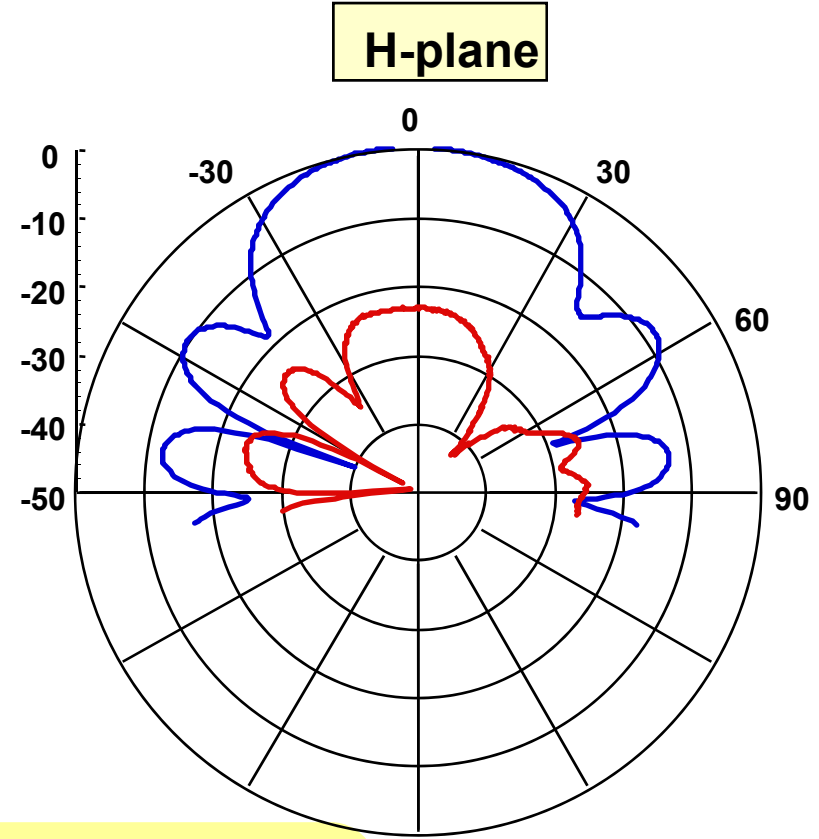
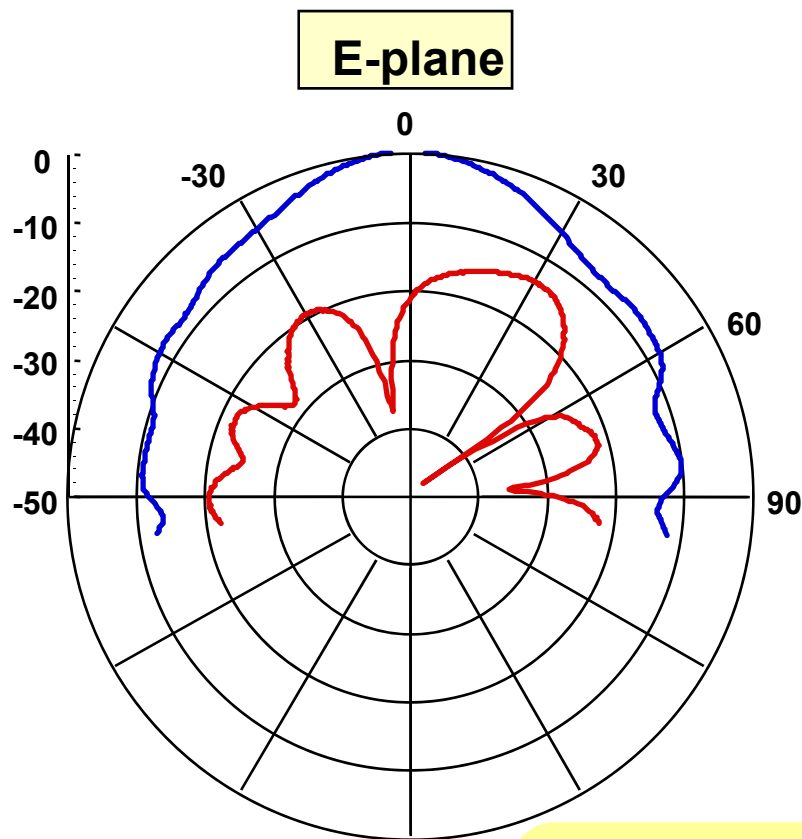
**Exponentially tapered slot**



**Feeding network: Marchand balun**

# Measured Radiation Patterns of Vivaldi Antenna

$w = 9 \text{ cm}$ ,  $l = 7 \text{ cm}$



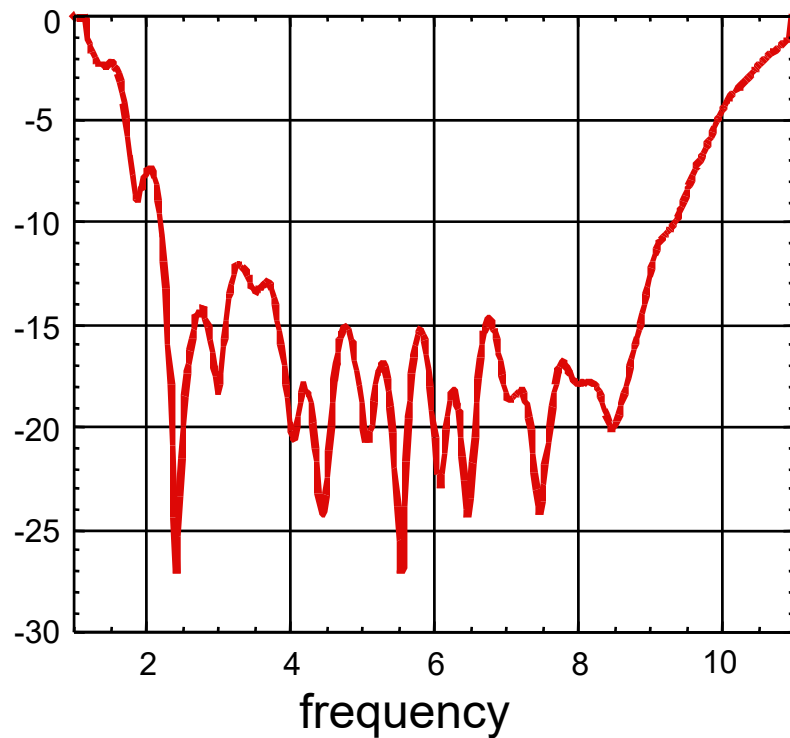
$f = 3\text{GHz}$

— Co-polarisation  
— Cross-polarisation

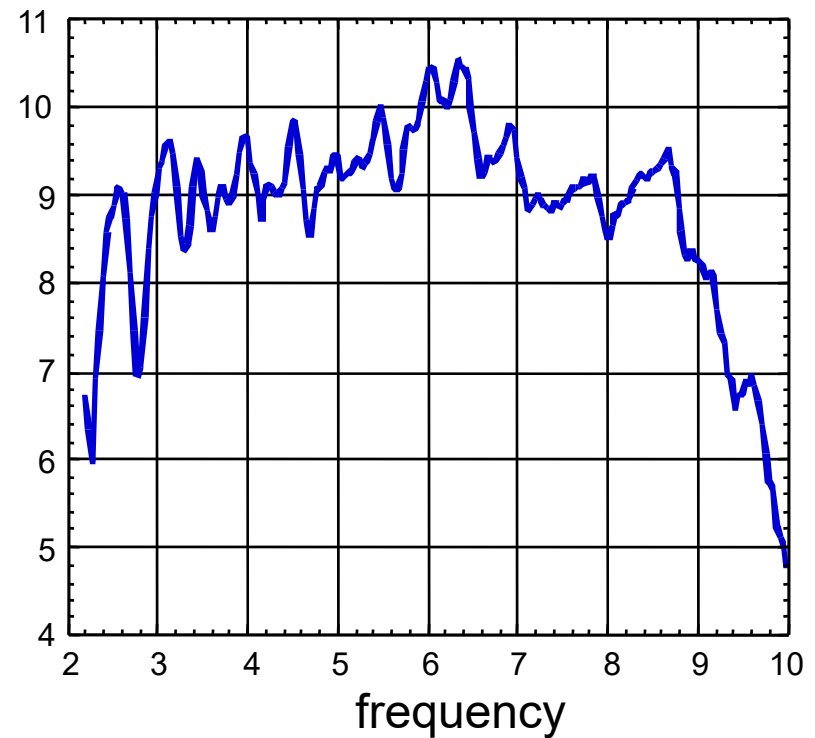
# Reflection Coefficient $S_{11}$ and Gain $G$ of Vivaldi Antenna

$w = 9 \text{ cm}$ ,  $l = 7 \text{ cm}$

$S_{11}$

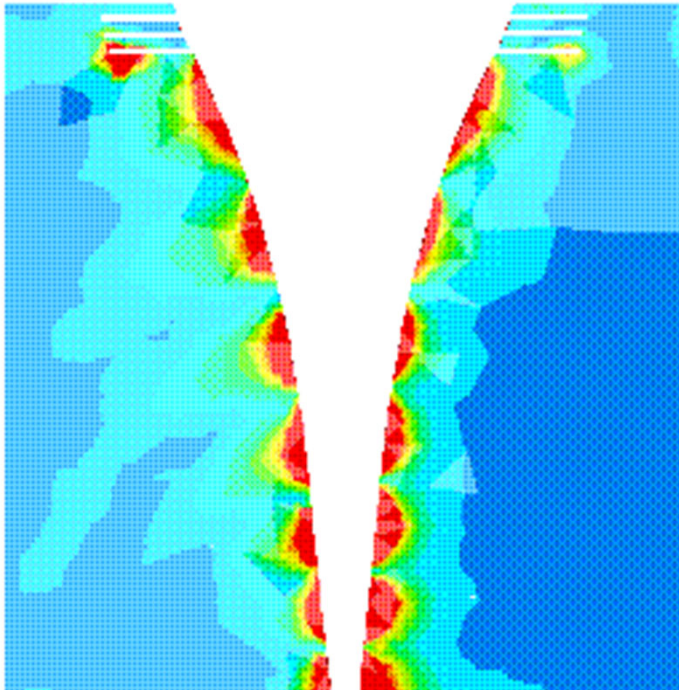


gain





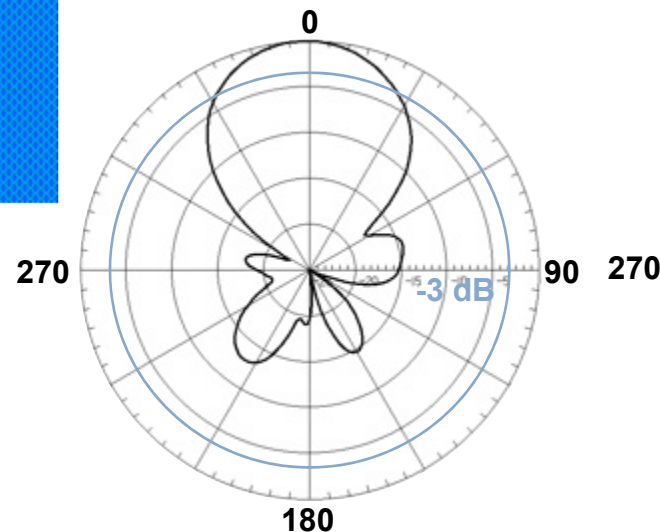
# Vivaldi Antenne mit Korrugationen



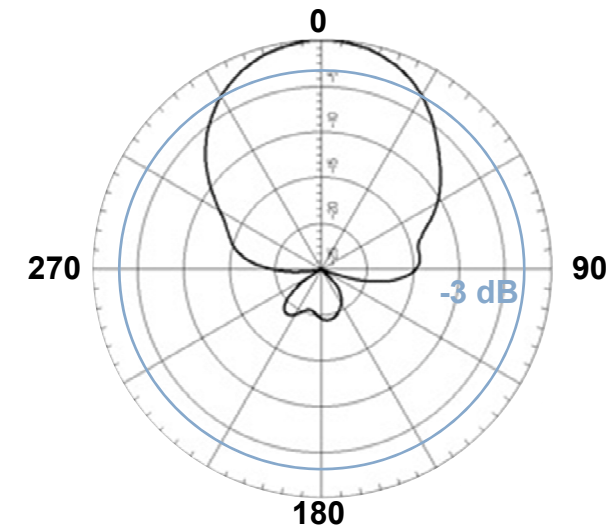
Auslöschung von Randströmen durch Korrugationen

Transformation eines Kurzschlusses in einen Leerlauf

**E-Ebene**



**H-Ebene**



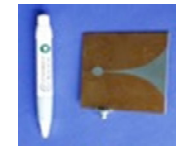
$$G_i = 9 \text{ dB}$$

$$\theta_{3\text{dB},E} = 60^\circ$$

$$\theta_{3\text{dB},H} = 60^\circ$$



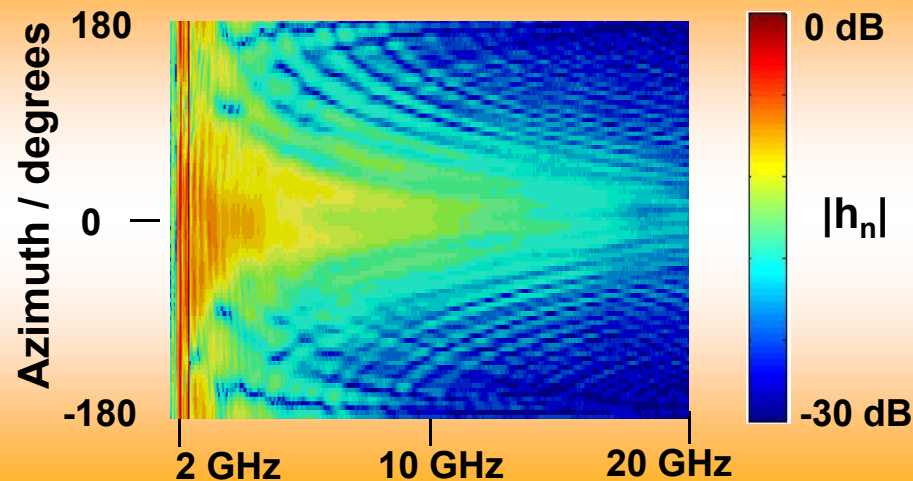
# Vivaldi Antenne mit Pulsansteuerung



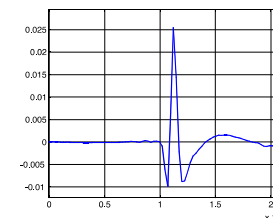
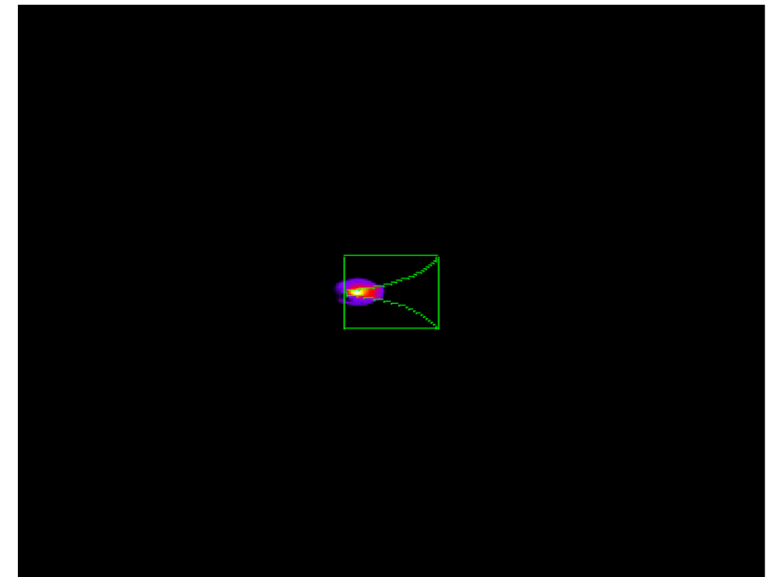
Antennas are **dispersive elements**. Radiation characteristics depend on frequency!

➔ UWB antenna characterisation in frequency and time domain.

## Example: Vivaldi Antenna



Anregung

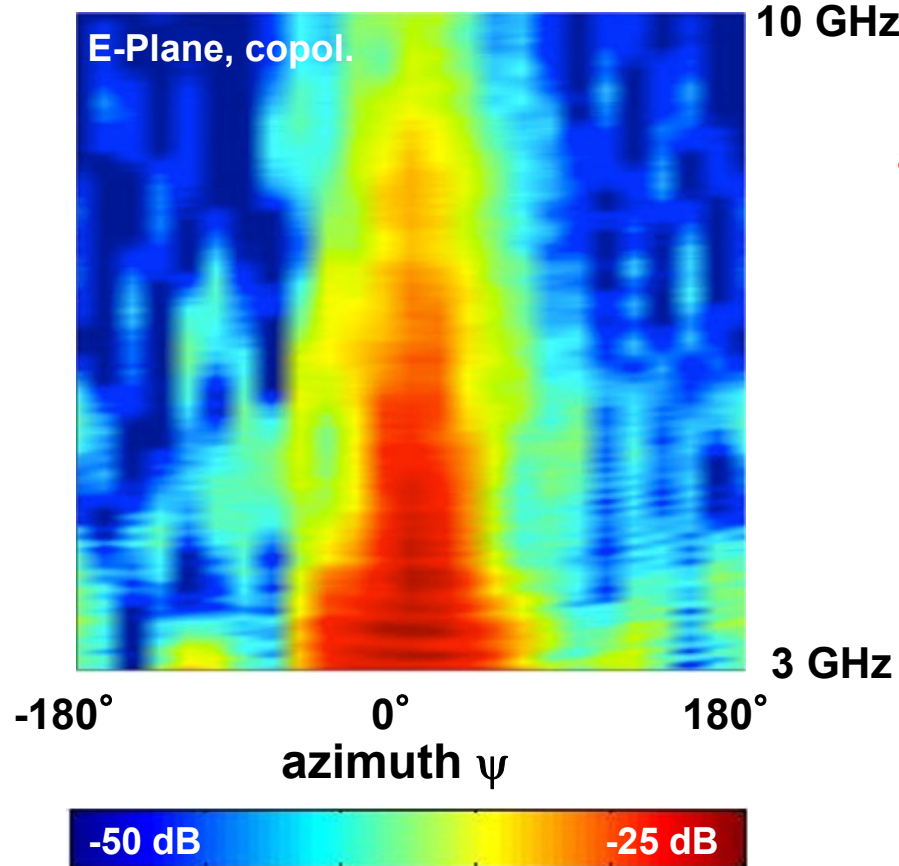


Antwort

# Measured Transfer Function $H_n$ and Gain



Transfer function  $|H_n(f, \psi)|$



**Transfer function:**

$$\vec{H}_n(f, \theta, \psi)$$

â linear model for radiated far field

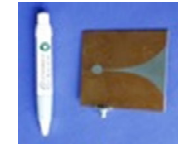
depends on:

- direction
- polarization
- frequency

**Antenna gain relation:**

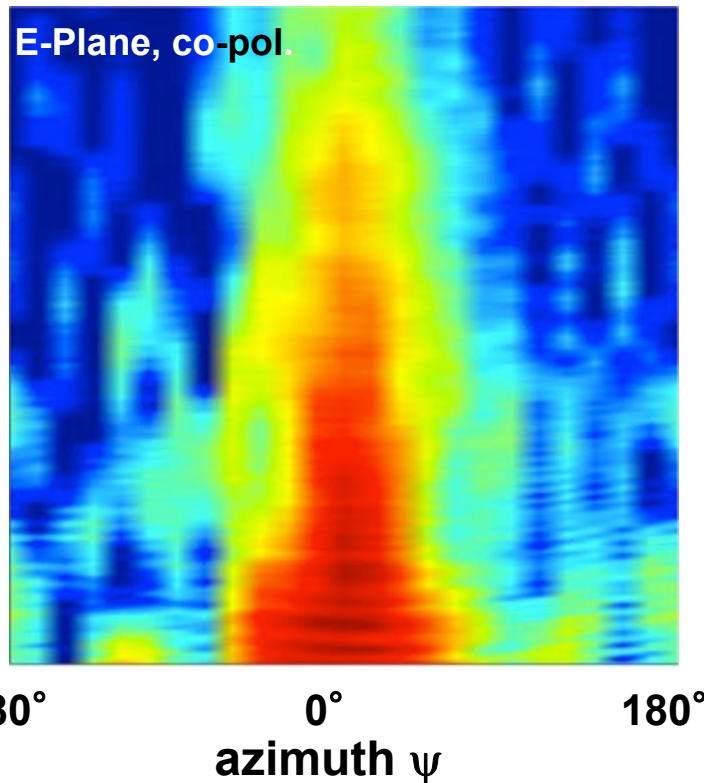
$$G(f, \theta, \psi) = \frac{4\pi f^2}{c^2} |\vec{H}_n(f, \theta, \psi)|^2$$

# Measured Transfer Function $H_n$ and Gain

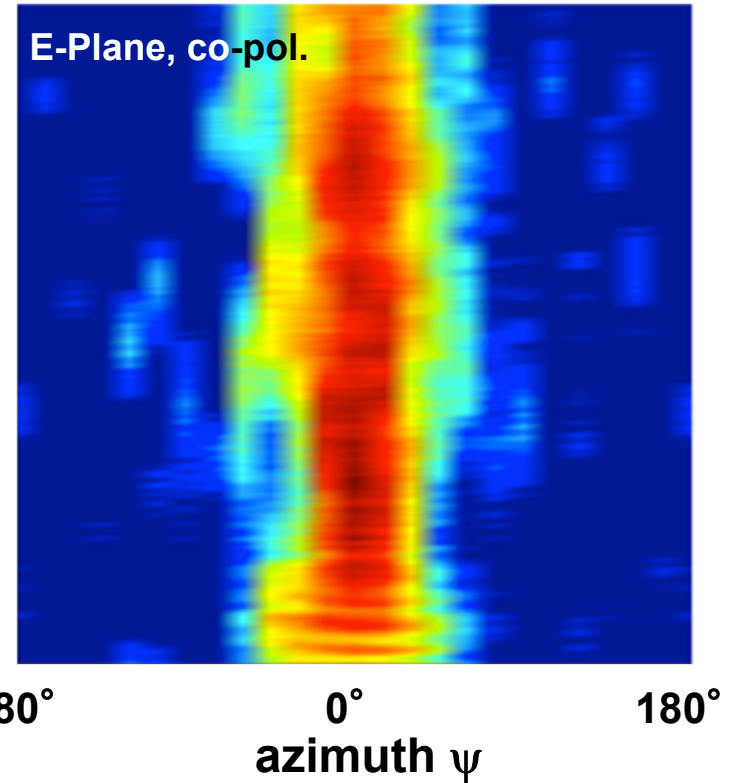


**Transfer function**  $|H_n(f, \psi)|$

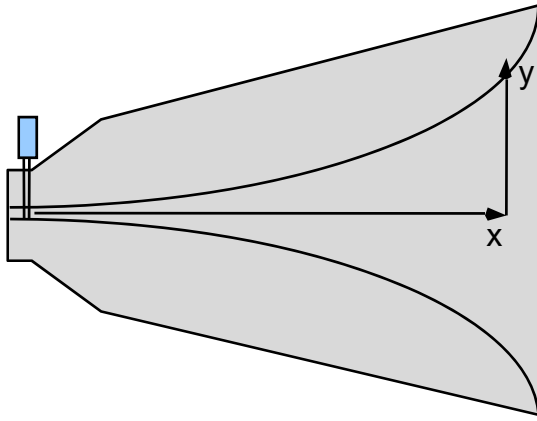
**Gain**  $G(f, \theta, \psi) = \frac{4\pi f^2}{c^2} \left| \vec{H}_n(f, \theta, \psi) \right|^2$



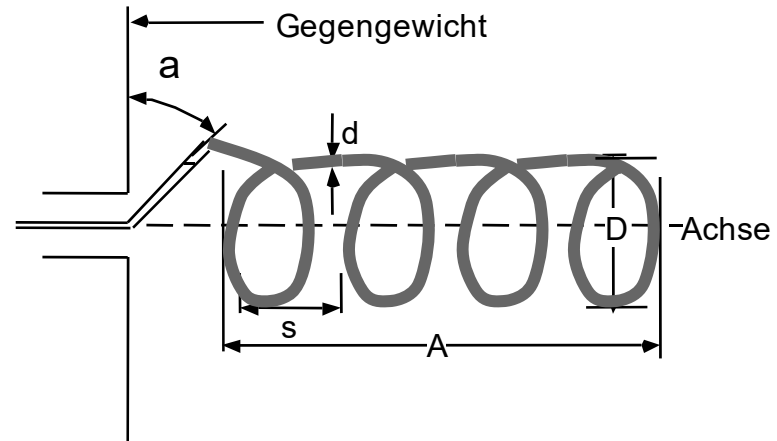
10 GHz



3 GHz

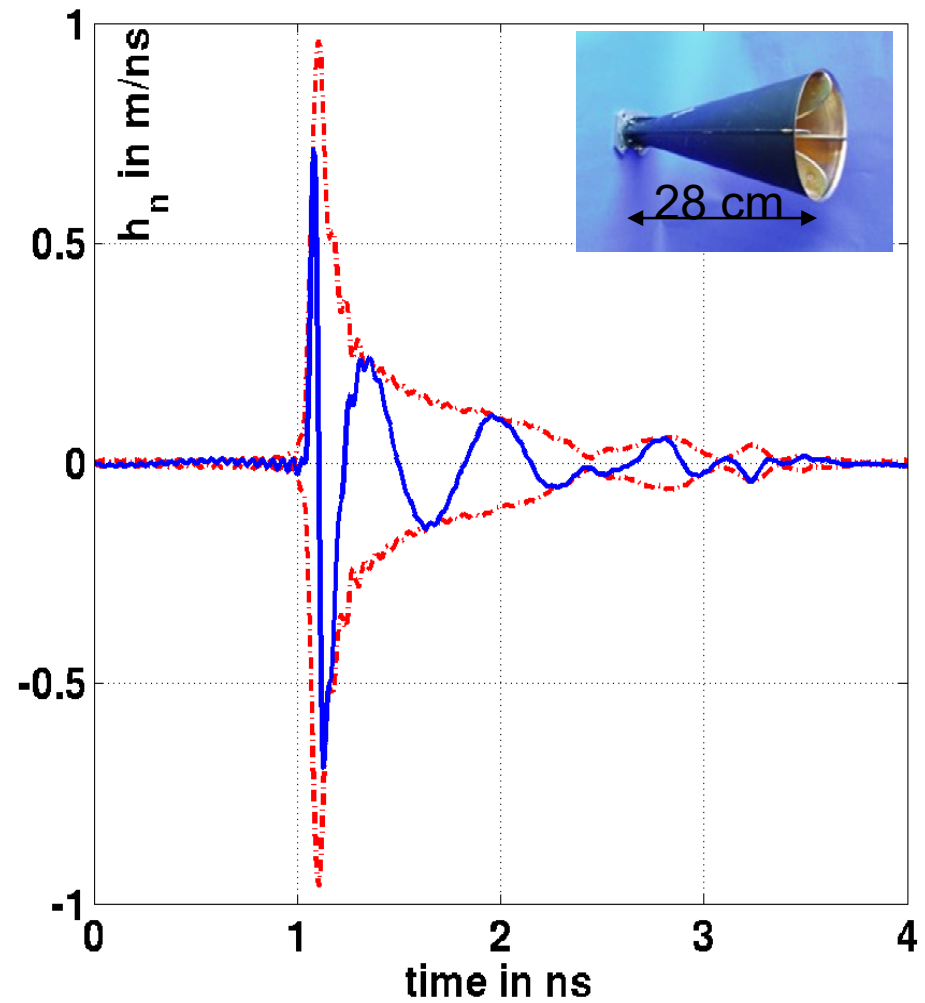
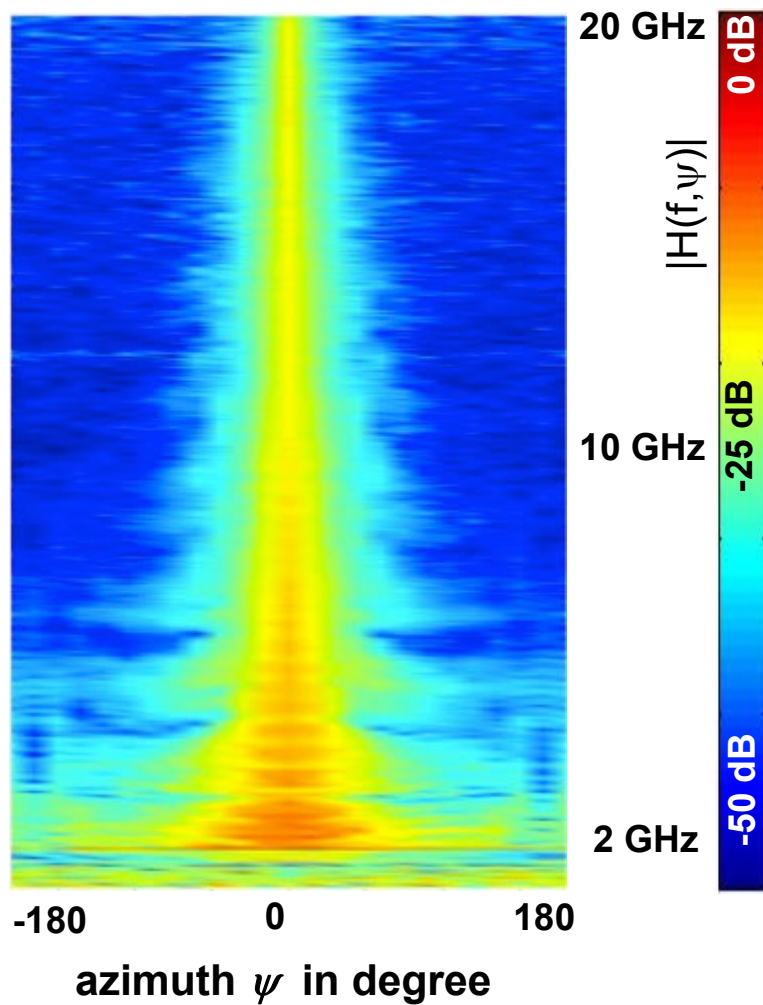


**Exponential Hornantenne**



**Wendelantenne**

# UWB Horn-Antenna Transfer Function $H(f, \psi)$





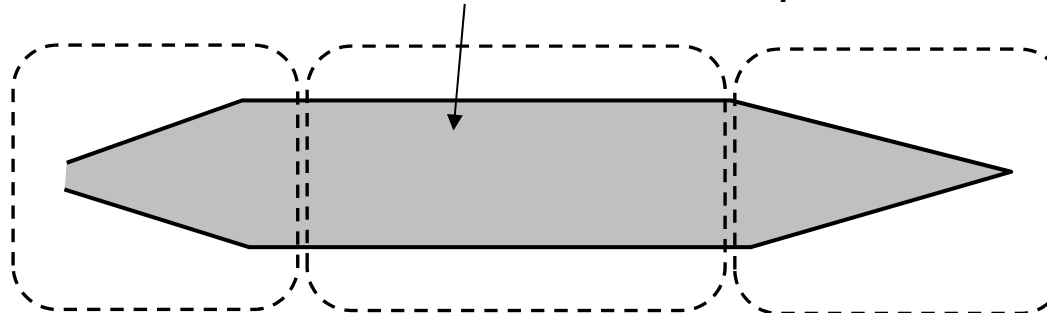
# Dielektrischer Stabstrahler

by Thomas Zwick

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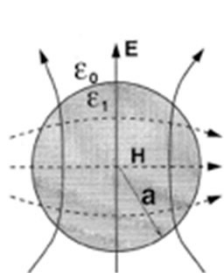
**Dielektrikum z.B. Teflon  $\epsilon_r=2.08$**



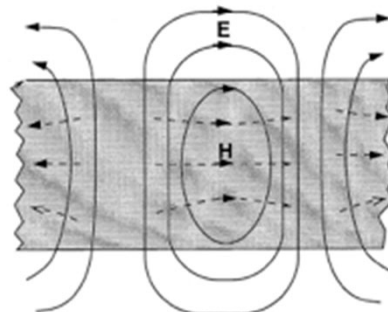
**Speisung**

**Wellenleiter**

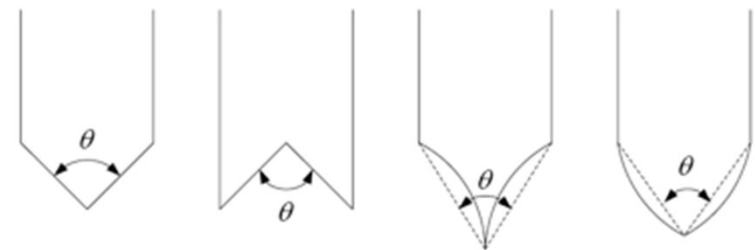
**Abstrahlung**



(a) Cross-Section View



(b) Side View

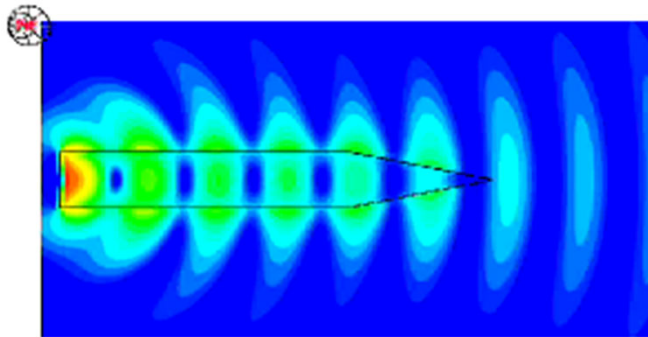


**Formen des Strahlers  
(üblich ein Konus)**

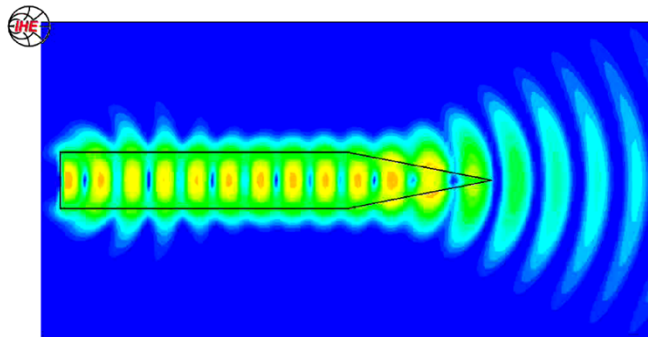
***HE<sub>11</sub>-Mode in Waveguide-Section***



# Abstrahlung



**Elektrisches Feld bei:**  
**3 GHz**

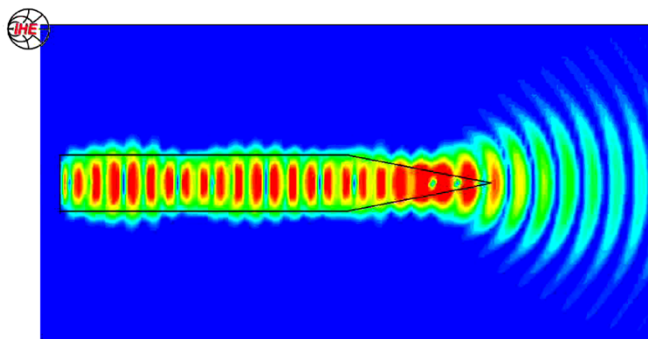


**5.5 GHz**

**Sehr große Bandbreite**

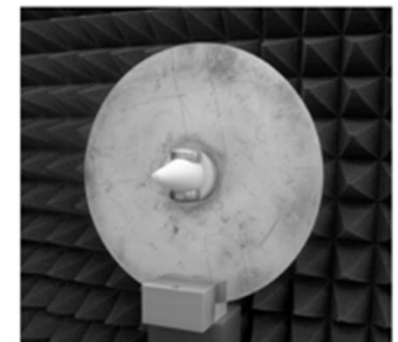
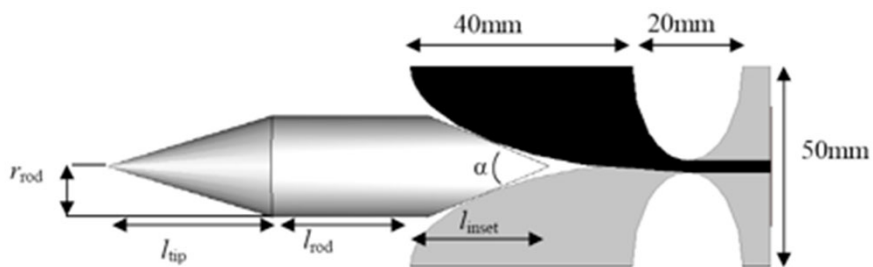
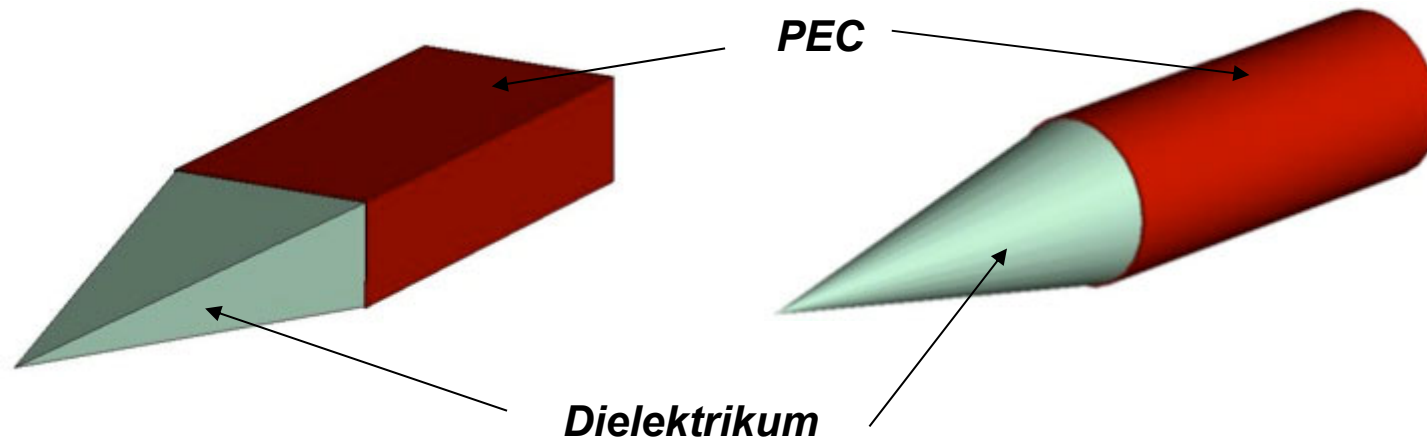
**Hohe Direktivität**

**Konstante Richtcharakteristik  
in breiten Frequenzbereich**



**9 GHz**

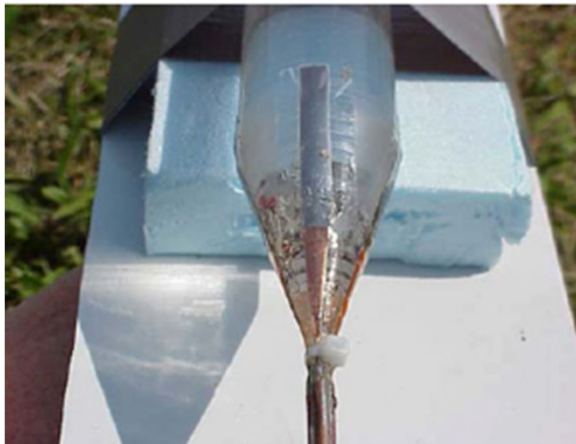
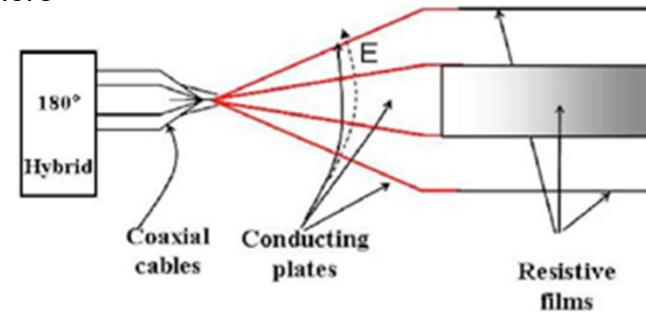
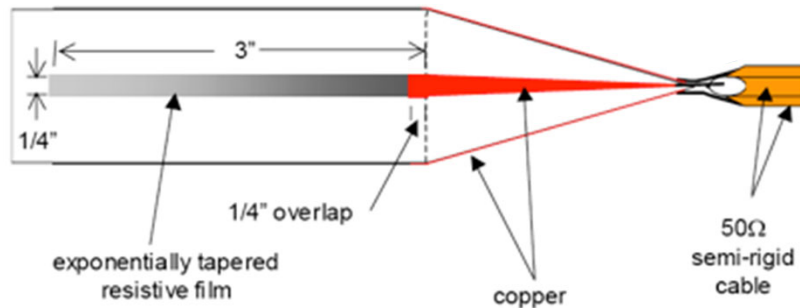
## Hohlleiter



Quelle: IEEEExplore

# Differentielle Speisung

Quelle: IEFEXplore



Quelle: „Design of Dielectric Rod Antenna for Near Field Measurement“  
Kwan-ho Lee, Chi-Chih Chen, Fernando Teixeira and Robert Lee

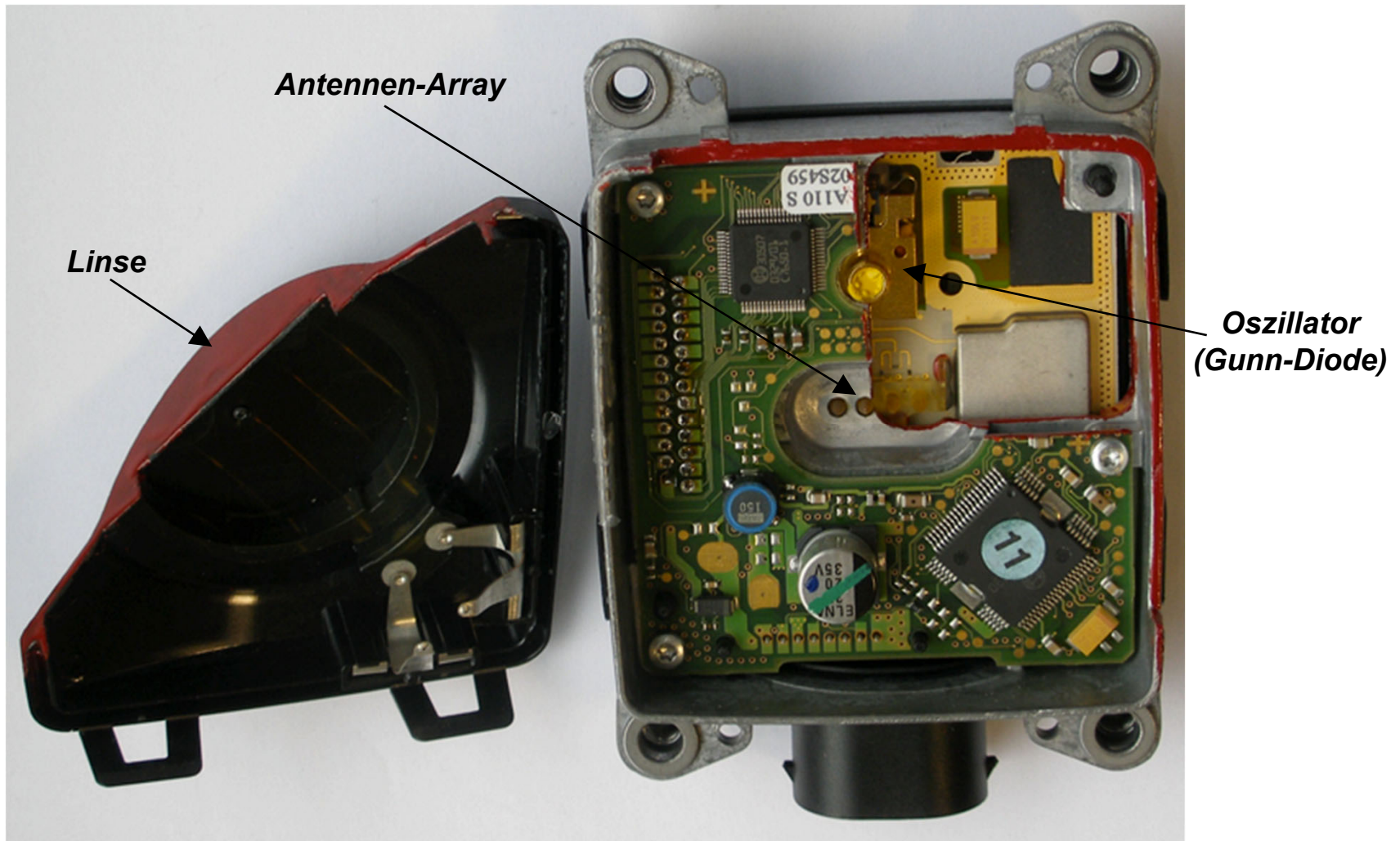
# Bosch ACC Radar



Courtesy  
Bosch



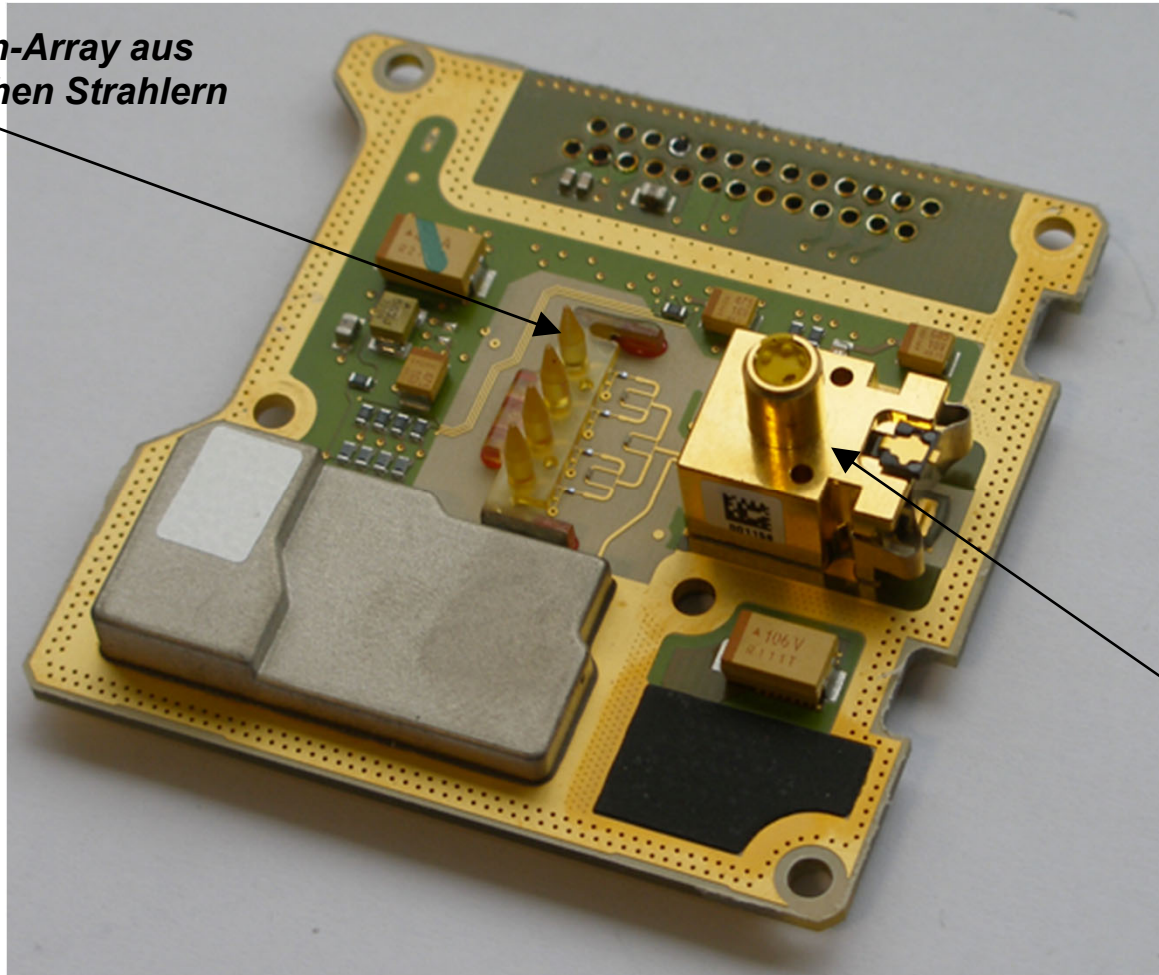
# Bosch ACC Radar - Antennensystem



**Courtesy Bosch**

# Bosch ACC Radar - HF Frontend

*Antennen-Array aus  
dielektrischen Strahlern*

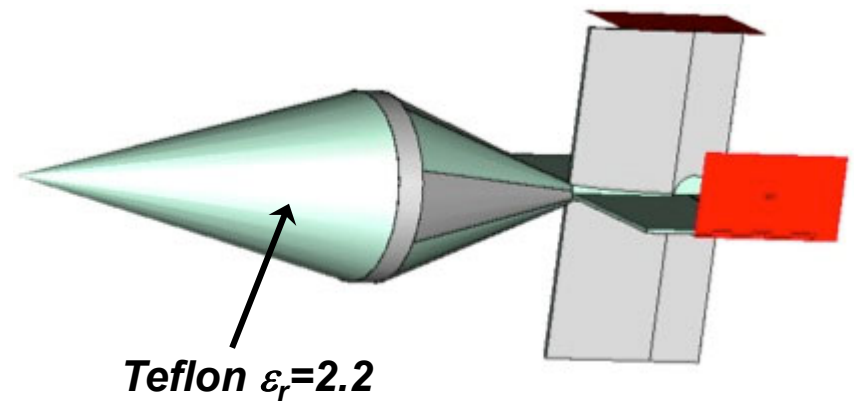
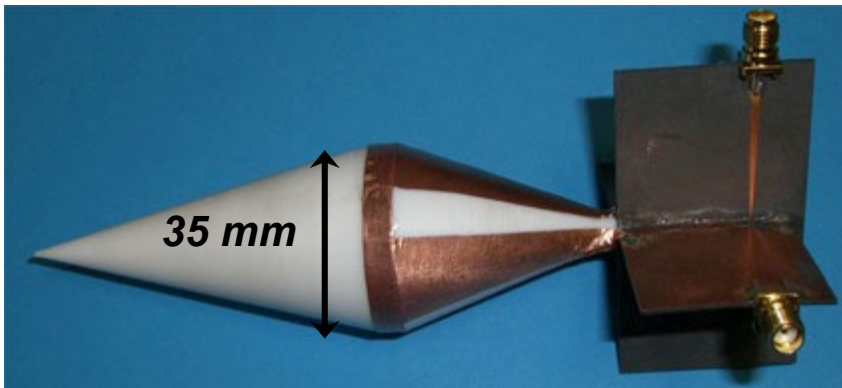
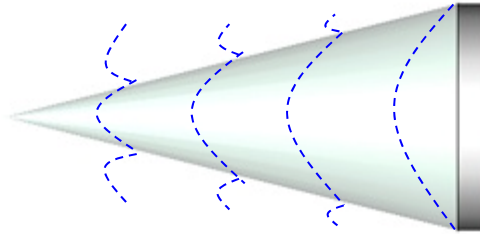


*Oszillator  
(Gunn-Diode)*

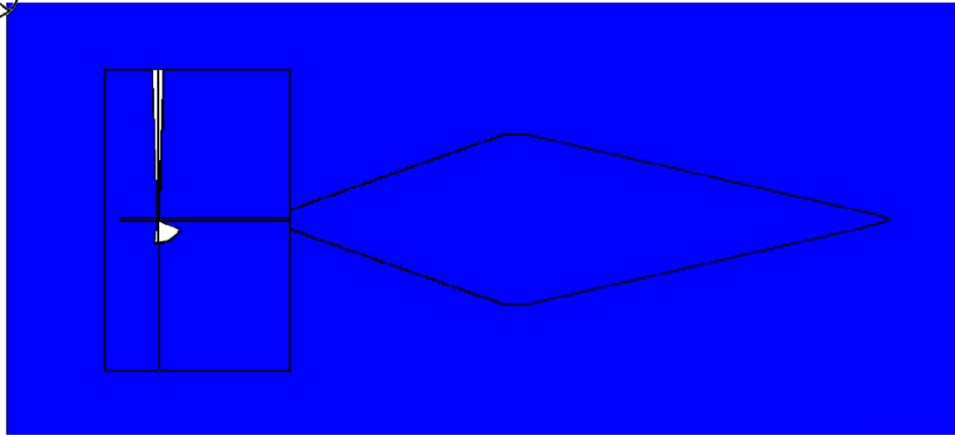
Courtesy Bosch



# Dual Polarized Dielectric Rod Antenna

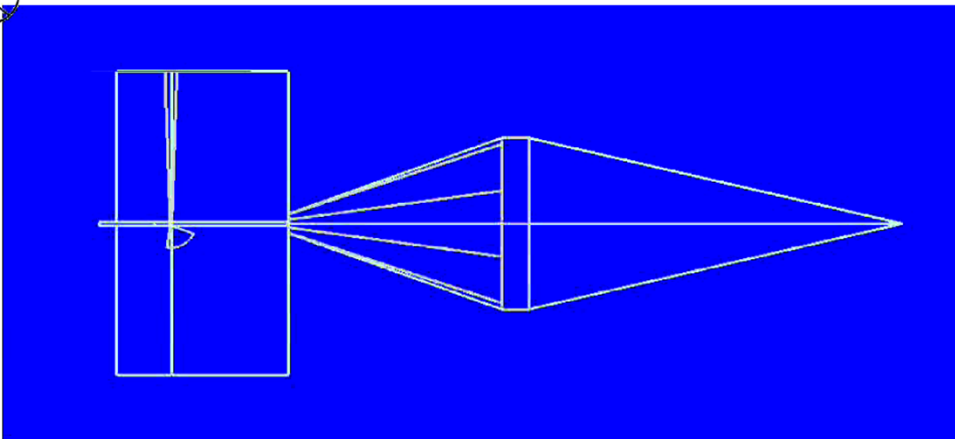
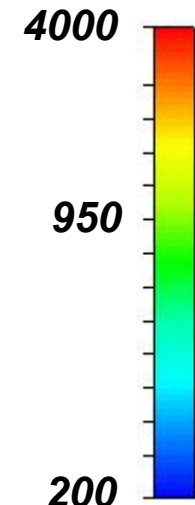


# Radiation Principle in Time Domain



*E-Plane*

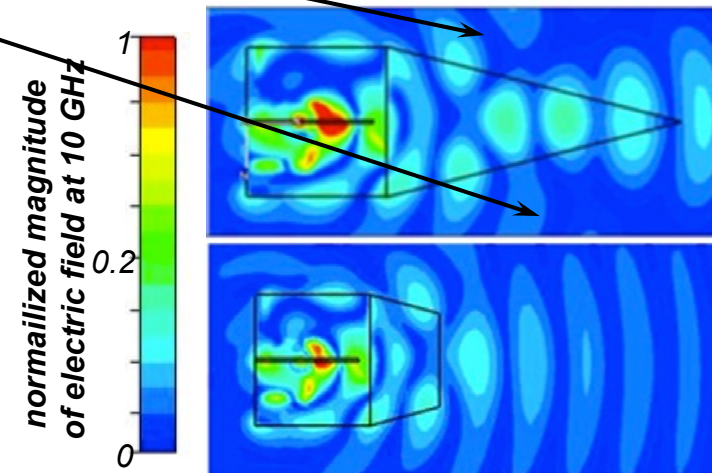
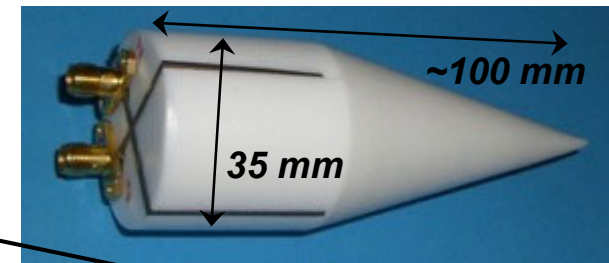
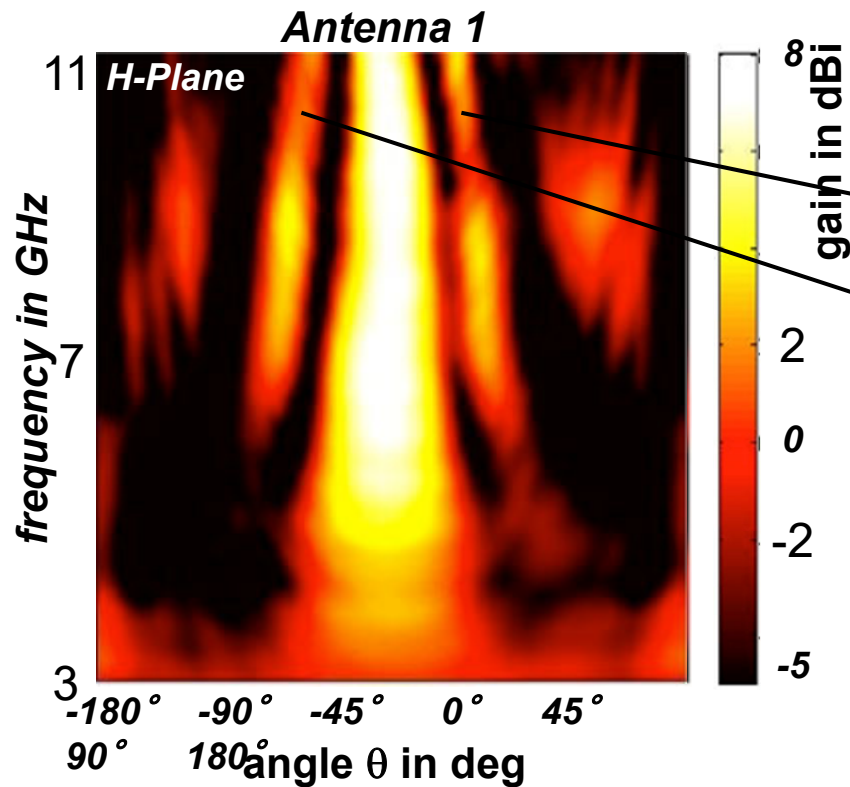
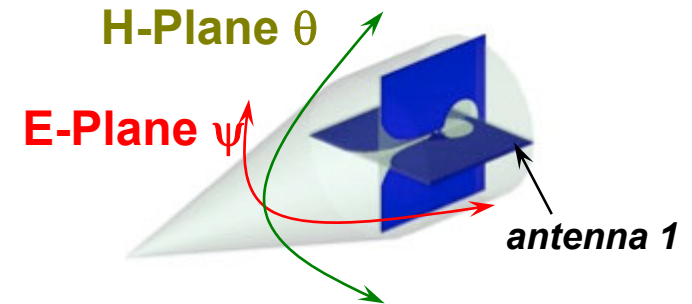
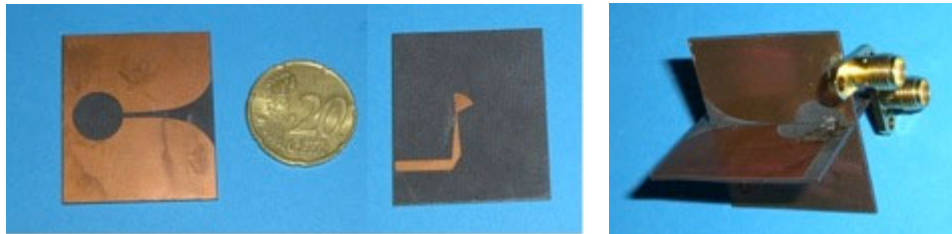
*E-Field in V/m*



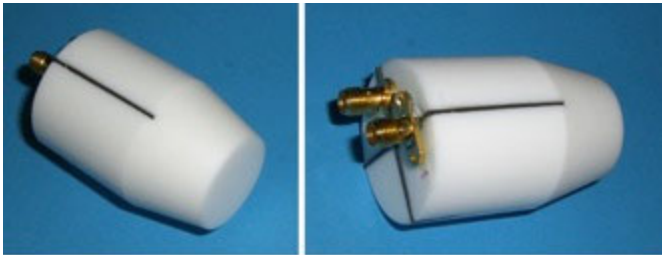
*H-Plane*



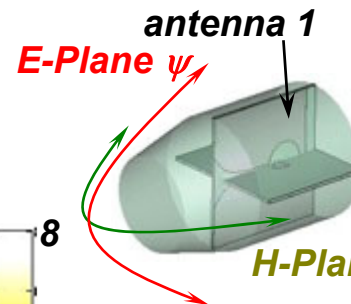
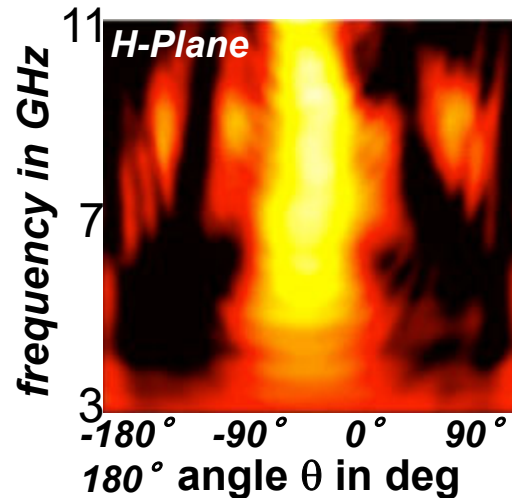
# Integration of the Feed



# Optimization of the Characteristics



- ✓ **very compact dimensions:**
  - Ø 35 mm
  - length 53 mm
- ✓ **suitable for the UWB antenna array**



**S-Parameter in dB**  
gain in dBi

